

Diffractors

≡ scattering from a hole in an opaque or conducting screen. A long confusing story ending in simple approximate formulas.

Starts with a scalar field pulse, for simplicity $\psi(x,t) = \psi(x) e^{-i\omega t}$, a solution of Helmholtz eqn.

$$(\nabla^2 + k^2)\psi = 0 \quad (c = ck)$$

Introduce the Green's fn $(\nabla^2 + k^2)G(x, x'; k) = -\delta^3(x-x')$

recall Green's theorem ($\phi = \psi$)

$$\int_V [G(x, x') \nabla'^2 \psi(x') - \nabla'^2 G(x, x') \psi(x')] d^3x' = \int_S [G(x, x') \mathbf{n}' \cdot \nabla' \psi(x') - \psi(x') \mathbf{n}' \cdot \nabla' G(x, x')] dA'$$

$$\nabla'^2 \psi = -k^2 \psi, \quad \nabla'^2 G = -k^2 G + \delta^3(x-x')$$

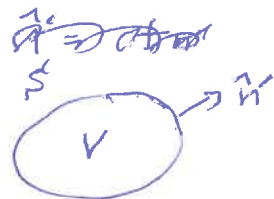
k^2 terms cancel. Integrate over S for

$$\psi(x) = \int_S dA' [G(x, x') \mathbf{n}' \cdot \nabla' \psi(x') - \psi(x') \mathbf{n}' \cdot \nabla' G(x, x')]$$

if $x \in V$, $\psi = 0$ otherwise

S' = closed surface, V is inside, $\mathbf{n}' = \text{outward normal to } S'$

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Jacobson 10.75 defines \mathbf{n}' pointing in so

sign flip on *.

Note this is not a solution - it's an integral eqn.
 Also, we started with a wave eqn - wave eqn's don't have solutions when we specify both ψ and $\frac{\partial \psi}{\partial n}$ on the boundary. (This is easy to fix: impose Dirichlet or Neumann b.c.'s - we'll come back to this.)

Now explicitly $G(x, x') = \frac{1}{4\pi R} \frac{e^{i\vec{k}\cdot\vec{R}}}{R}$ where $\vec{R} = \vec{x} - \vec{x}'$

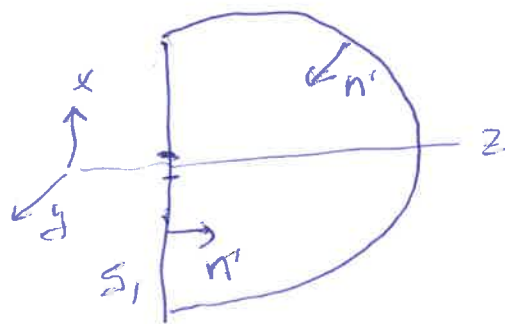
$$\vec{\nabla}' \frac{e^{i\vec{k}\cdot\vec{R}}}{R} = \left(i\vec{k} - \frac{1}{R} \right) \frac{e^{i\vec{k}\cdot\vec{R}}}{R} \vec{\nabla}' R \quad \text{neglect } \frac{1}{R}$$

$$\vec{\nabla}' R = \nabla' \sqrt{(\vec{x} - \vec{x}')^2} = -\frac{\vec{R}}{R} \quad \text{So}$$

$$\psi(x) = -\frac{1}{4\pi} \int_{\Sigma} dA' \hat{n}' \cdot \left[\vec{\nabla}' \psi(x') + \frac{\vec{R}}{R} \left(i\vec{k} - \frac{1}{R} \right) \psi(x') \right]$$

- sign - inner normal for \hat{n}'

Now specialize to case where Σ is an infinite plane screen Σ_1 (with an aperture) plus an infinite hemisphere Σ_2 . On Σ_2 , $\psi \sim \frac{e^{i\vec{k}\cdot\vec{r}'}}{r'}$



$$\vec{\nabla}' \psi \sim i\vec{k} \frac{e^{i\vec{k}\cdot\vec{r}'}}{r'} \rightarrow \frac{\vec{R} \cdot \hat{n}'}{R} = -1$$

$$\int_{\Sigma_2} \hat{n}' \cdot \left[i\vec{k} - \frac{1}{R} \right] \frac{e^{i\vec{k}\cdot\vec{r}'}}{r'} dA' = 0$$

$\frac{1}{R} \text{ term}$

Kirchhoff integral formula

$$\psi(x) = -\frac{1}{4\pi} \int_{S_1} dA' \frac{e^{ikR}}{R} \hat{n}' \cdot \left[\nabla' \psi(x') + \frac{\vec{R}}{R} \psi(x') \right]$$

$$= -\frac{1}{4\pi} \int_{S_1} dA' \left[\hat{n}' \cdot \nabla' \psi(x') + \psi(x') \hat{n}' \cdot \frac{\vec{R}}{R} \right]$$

(putting the Greens fn back on -)

Desire - specify information on S_1 , compute radiation far away (i.e. specify ψ on aperture)

Issues: 1) math consistency
2) practical calculations
3) scalar \rightarrow vector

1) Consistency - need Dirichlet or Neumann b.c.

either $\psi = \psi_D$ with $\psi_D = 0$ on S_1

or
 $\psi = \psi_N$ with $\frac{\partial \psi_N}{\partial n'} = 0$ on S_1

trick - S_1 is a flat plane ^{at $z=0$} - use images

$$\psi_D(x, x') = \frac{1}{4\pi} \left[\frac{e^{ikR}}{R} - \frac{e^{ikR''}}{R''} \right]$$

$$R = |x - x'| = \sqrt{(x-x')^2 + (y-y')^2 + (z-z')^2}$$

$$R'' = |x - x''| = \sqrt{(x-x'')^2 + (y-y'')^2 + (z-z'')^2}$$

$\vec{x}'' = \hat{i}x' + \hat{j}y' - \hat{k}z'$ - mirror image of x'

$$\psi_N = \frac{1}{4\pi} \left[\text{"} + \text{"} \right]$$

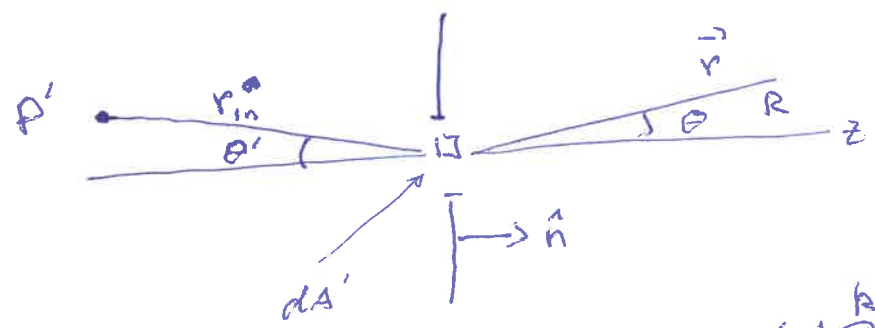
and evaluate on S_1 - at $z'=0$ - so $R=R''$

∞ $\psi_D(x) = \frac{1}{4\pi} \int_{S_1} dA' \psi'(x') \frac{2 \hat{z} \cdot \vec{R}}{R} \frac{e^{-ikR}}{R}$

$\psi_N(x) = \frac{1}{4\pi} \int_{S_1} dA' \frac{e^{-ikR}}{R} 2 \hat{n}' \cdot \nabla' \psi'(x')$

Kirchhoff - average of the two (inconsistent)

Not much difference, practically - consider a source at P' at $z=0$, absence at large R



on the aperture $\psi_0(r') = \frac{e^{i k r_{in}}}{r_{in}}$ - spherical wave;

$r'(r_{in}) \approx$ distance $r_{in} - \hat{n}' \cdot r'$ (r' on the aperture)
 $\hat{n}' \cdot \nabla' \psi_0(r') = \hat{z} \cdot \nabla' \frac{e^{i k r_{in}}}{r_{in}} = i k \hat{z} \cdot \hat{r}'_{in} \frac{e^{i k r_{in}}}{r_{in}}$
 $= i k \frac{e^{i k r_{in}}}{r_{in}} \cos \theta'$

$\frac{1}{2} \cdot \vec{R} / R = \cos \theta$

D: $\psi(r) = \frac{k}{2\pi i} \int_{S_1} \frac{e^{-ikr}}{r} \cos \theta \frac{e^{i k r_{in}}}{r_{in}} dA'$

N $\frac{k}{2\pi i} \int \frac{e^{-ikr}}{r} \cos \theta' \frac{e^{i k r_{in}}}{r_{in}} dA'$

K $\frac{k}{2\pi i} \int \frac{e^{-ikr}}{r} \frac{\cos \theta + \cos \theta'}{2} \frac{e^{i k r_{in}}}{r_{in}} dA'$

Huygens (even more inconsistent) 1

The physics point is that if the aperture is reasonably large, $\frac{\Delta x}{\lambda} \gg 1$, and the incident beam is reasonably normally incident, the diffraction pattern will peak forward:

$\cos \theta \sim 1$, $\cos \theta' \sim 1$. ~~Also~~ The integral is dominated by the $e^{i k r}$ $e^{i k r'}$ term.

~~The~~ The discussion in the optics literature is a bit more general / complicated than in Jackson. We need $\psi(x')$ in the aperture. It ~~is~~ comes from a source on the far side of the opening.

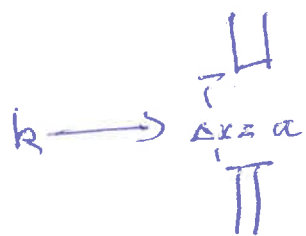
$$* \quad \psi(x') = \int_{\text{source}} \frac{E(x, x_0)}{r} \psi(x_0)$$

~~the~~ $E(x, x_0)$ propagates source to aperture. This is not discussed in Jackson - nor does he discuss possibility that $\psi(x')$ is not uniform across the aperture. To use $*$, need $\Delta x \gg \lambda$ so aperture does not affect most of the incoming wave.

You can see, things are starting to get ~~complicated~~ complicated ...

There are two important special cases which we can motivate by uncertainty principle arguments:

At aperture, beam has width $\Delta x = a$. This



introduces a $\Delta k_x \sim \frac{1}{\Delta x}$

$$(\Delta k_x \Delta x \sim 1) -$$

beam spreads.

Look out a distance r :



~~Combine with intrinsic width of beam~~

$$\Delta x_r = \frac{\Delta k_x}{k} r = \frac{1}{ak} r$$

Beam spreads - combine spread with intrinsic

width, $\Delta x_r \sim a$

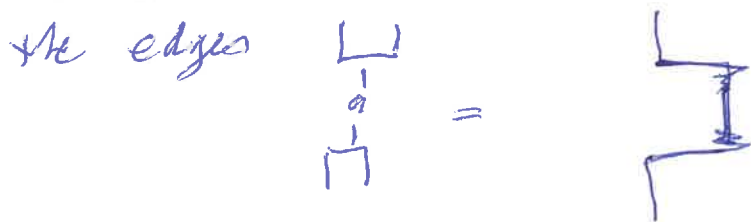
$$\Delta x_{TOT} = \left[a^2 + \left(\frac{r}{ak} \right)^2 \right]^{1/2}$$

Two extreme limits!

$$1) \Delta x_{TOT} \approx a \text{ if } \frac{r}{ak} \ll a \text{ or } \frac{r}{k} \ll a^2$$

$$\text{or } \left(k = \frac{2\pi}{\lambda} \right) \underline{\lambda r \ll a^2}$$

This is called the Fresnel limit - basically, image given by geometric optics w/ ripples on the edges



2) $\phi \frac{r}{ak} \gg a$ or $\lambda r \gg a^2$, ~~no~~ beam spread is all $\Delta k_x \Delta x = 1$. This is called Fraunhofer diffraction



Mathematical difference between the 2 is how e^{-ikR} is expanded

$$R = |x - x'| \quad ; \quad |x| = r, \quad |x'| = r' \approx a$$

$$kR = kr - k\hat{n} \cdot \vec{x}' + \frac{k}{2r} \left[r'^2 - (\hat{n} \cdot \vec{x}')^2 \right]$$

$$\text{size} \quad kR + \left[ka \approx \frac{a}{\lambda} \right] + \left[\frac{ka^2}{r} \approx \frac{a^2}{\lambda r} \right] + ka \left(\frac{a}{r} \right)^2 + O\left(\frac{ka^3}{r^2}\right)$$

If $r \gg a$, last term is always small

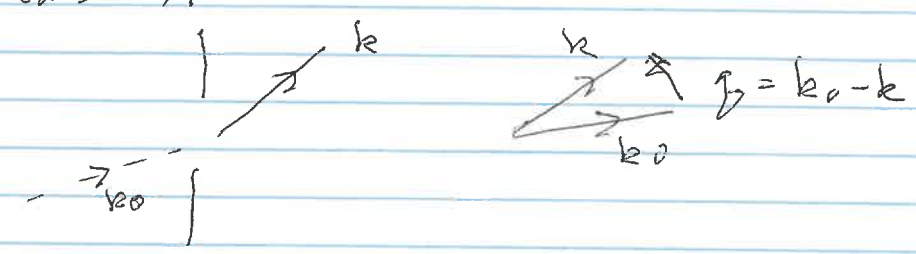
Fraunhofer is $\frac{a^2}{\lambda r} \ll 1$ so only keep first 2

$$\frac{e^{-ikR}}{R} = \frac{e^{-ikr}}{r} e^{-ik\hat{n} \cdot \vec{x}'}$$

Just like the far field limit for antenna or scatterer.

Thorn + Blanford have pictures of patterns for $\lambda r \ll a^2$ to $\lambda r \gg a^2$.

With $\psi_0(x') = A e^{i \vec{k}_0 \cdot \vec{x}'}$



$$\psi_D = \frac{k}{2\pi i} \frac{e^{i k r}}{r} \cos \theta \cdot A \int_{\text{aperture}} e^{i \vec{\gamma} \cdot \vec{x}'} dA'$$

Easy example - square hole of size L, normal incidence - $\vec{k}_0 = (0, 0, k)$

$$\vec{x}' = (x', y', 0)$$

$$\vec{k} = (k_x, k_y, k_z)$$

$$\vec{x}' \cdot \vec{k} = k_x x' + k_y y'$$

$$\int_{\text{aperture}} dA' e^{i \vec{k} \cdot \vec{x}'} = \int_{-L/2}^{L/2} dy' e^{i k_y y'} \int_{-L/2}^{L/2} dx' e^{i k_x x'}$$

$$= L^2 \left[\frac{\sin k_y L/2}{k_y L/2} \right] \left[\frac{\sin k_x L/2}{k_x L/2} \right]$$

$|\psi|^2 = \text{intensity}$ - look along one axis -
 $k_y = 0 \Rightarrow k_x = k \sin \theta \sim k \theta$

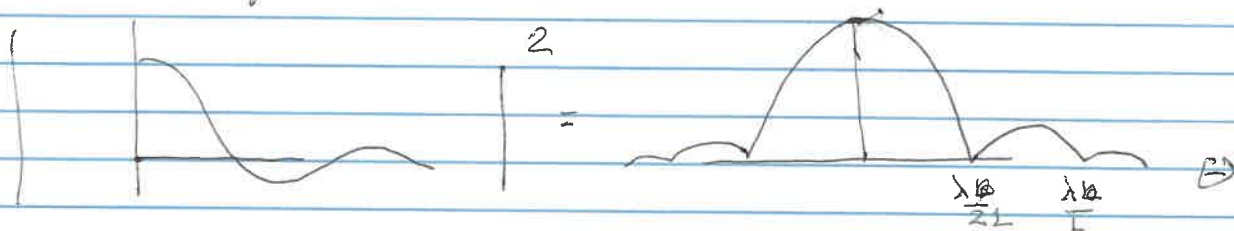
$$I \sim \frac{\sin^2 \frac{kL\theta}{2}}{\left(\frac{kL\theta}{2}\right)^2}$$

nodes at $\frac{kL\theta}{2} = \pi, 2\pi, \dots = \frac{2\pi L\theta}{\lambda} = \pi, 2\pi, \dots$

envelope falls as $(kL\theta)^2$

$I(\theta)$

$$\theta \approx \frac{\lambda}{2L} \cdot 5.3$$



everything happens at small $\theta \sim \frac{\lambda}{L}$

Note also - a k_x is induced by the aperture

$$k_x = k \sin \theta = \Delta k_x = k\theta$$

$$\Delta x \sim L$$

$\Delta k_x \Delta x \sim 1$ - (RL $\theta \sim 1$)
~~application~~ restricting size of wave induces
 nonzero wave number -

classical version of uncertainty principle.

\Rightarrow resolving power of optical ~~images~~ ^{devices}...

Note also - if $\frac{\lambda}{L} \rightarrow \text{large}$ ($\frac{L}{\lambda} \rightarrow \text{small}$)

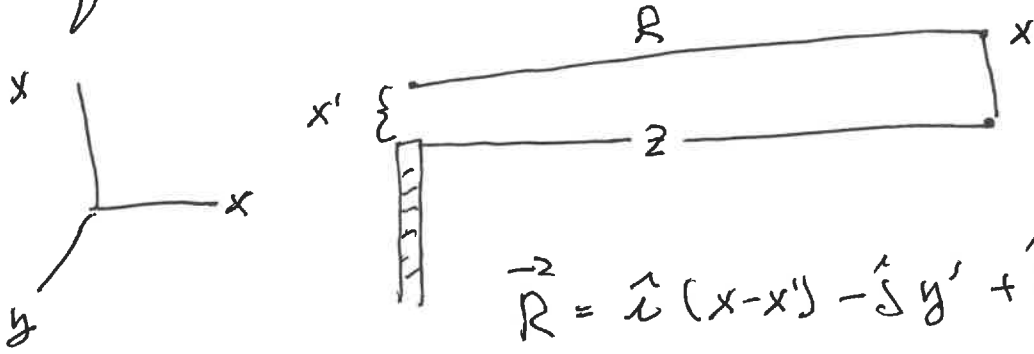
the diffraction minimum moves out to $\theta = \frac{\pi}{2}$

JDJ: "The assumption of unperturbed fields in

the aperture breaks down."

2) Fresnel diffraction keeps the $\frac{ka^2}{r} \gg 1$ term.

Best described by example - prob. 2 of homework
Useful to eliminate the linear term with a change of variables



$$\vec{R} = \hat{i}(x-x') - \hat{j}y' + \hat{k}z$$

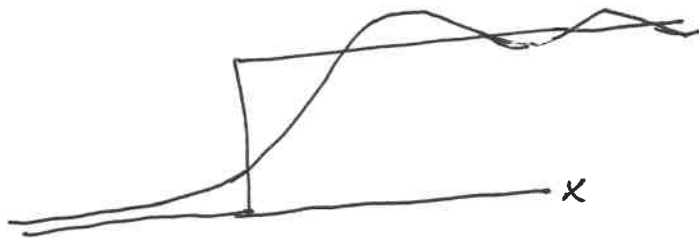
$$R = [(x-x')^2 + y'^2 + z^2]^{1/2}$$

$$\approx z + \frac{1}{2z} [(x-x')^2 + y'^2]$$

and $\hat{n} \cdot \hat{R} = \hat{n}' \cdot \hat{z} = 1$

$\psi_0(x') = I_0^{1/2} e^{ik_0 x'} \rightarrow I_0^{1/2}$ for normal incidence

$$\psi(x) = \frac{k}{2\pi i} \frac{e^{ikz}}{z} I_0^{1/2} \int_0^\infty dx' \int_{-\infty}^\infty dy' \times \exp\left\{i\frac{k}{2} \left[\frac{(x-x')^2}{2z} + \frac{y'^2}{2z} \right]\right\}$$



Intensity rises as the observer moves above the knife-edge

Vector formula is called the "vector Smythe-Kerckhoff formula"

$$\vec{E}(x) = \frac{1}{2\pi} \vec{\nabla} \times \int_{\text{Aperture}} \frac{e^{-ikR}}{R} \hat{n} \times \vec{E}(x') dA'$$

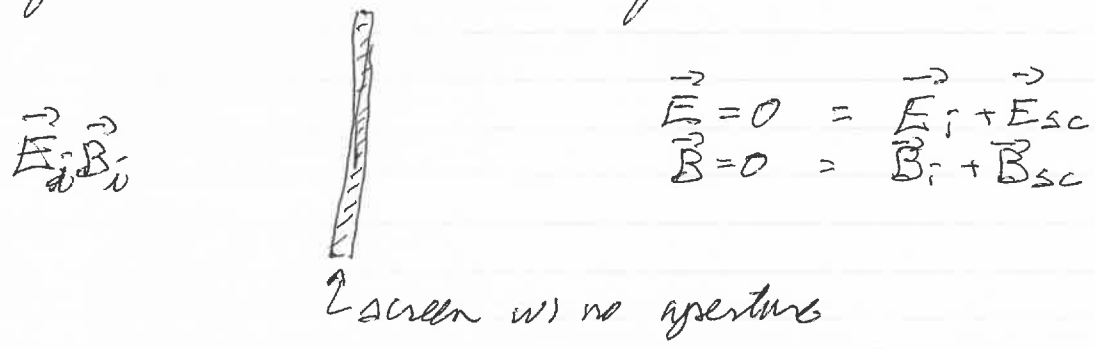
and in Fraunhofer limit

$$\vec{E}(x) = \frac{ik}{2\pi} E_0 \frac{e^{-ikr}}{r} \hat{n} \times (\hat{z} \times \vec{E}_0) \int_{\text{Aperture}} dA' e^{i(\vec{k}_0 - \vec{k}) \cdot \vec{x}'}$$

what's new: polarization info

long, difficult derivation: physics issues are basically

- ① due to fact that, really, radiation does not just come from the hole - it comes from the walls. Think about it:



field from screen caused by charges + currents in screen

"official" derivation only for conducting screen

- ② We don't want to deal with the screen, we only want to deal with the hole, so lots of reworking - turns out, can only do this for \vec{E} ; \vec{B} involves integral over complementary region (the screen)

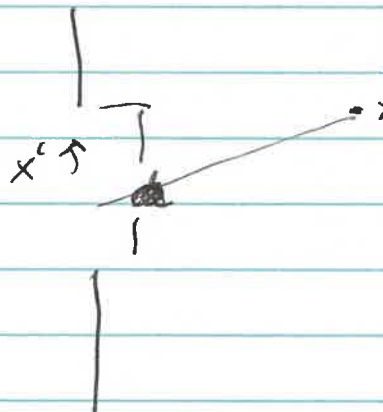
Example: Diffraction by Circular Aperture

Use the Smythe-Kirchhoff formula with

$$\vec{E}(x) = \vec{E}_0(x) \text{ the incident field}$$

$$\vec{E}(x) = \frac{1}{2\pi} \vec{\nabla}_x \int dA' \frac{e^{ikR}}{R} \hat{z} \times \vec{E}_0(x')$$

Fresnel's:



$$\frac{e^{ikR}}{R} = \frac{e^{ikr}}{r} e^{-ik\hat{n} \cdot x'}$$

$$\vec{\nabla} \rightarrow ik\hat{n}$$

$$\vec{E} = \hat{z} \times \vec{E}_0 e^{ik\hat{z} \cdot x'}$$

$$\vec{E}(x) = \frac{ik}{2\pi} \vec{E}_0 \frac{e^{ikr}}{r} \hat{n} \times (\hat{z} \times \vec{E}_0) \int_{\text{aperture}} dA' \exp i(\vec{k}_r - k\hat{n}) \cdot x'$$

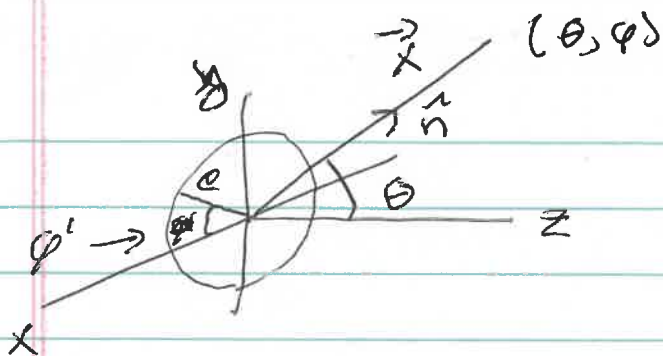
Let's assume $\vec{k}_0 = \hat{z} k_0$ normal incidence for simplicity.

Pick $\hat{z}_0 = \hat{x}$: $\hat{n} \times (\hat{z} \times \hat{x}) = (\hat{n} \times \hat{y})$

Aperture in x - y plane

Note $\vec{k}_0 \cdot x' = 0$

Focus on $I = \int_{\text{aperture}} e^{-ik\hat{x} \cdot x'} dA'$



$$\hat{n} = [\hat{x} \cos \varphi + \hat{y} \sin \varphi] \sin \theta + \hat{z} \cos \theta$$

$$x' = e' [\hat{x} \cos \varphi' + \hat{y} \sin \varphi']$$

$$0 < e' < a$$

$$\hat{n} \cdot \vec{x}' = e' \sin \theta \cos(\varphi - \varphi')$$

$$I = \int_0^a e' de' \int_0^{2\pi} d\varphi' e^{-ik e' \sin \theta \cos(\varphi - \varphi')}$$

Now it's just special functions

- shift variables to $d(\varphi - \varphi')$

$$- J_0(x) = \frac{1}{2\pi} \int_0^{2\pi} d\varphi' e^{\pm i x \cos \varphi}$$

$$x = k e' \sin \theta \equiv g e'$$

$$\vec{E}(x) = ik E_0 [\hat{n} \times \hat{y}] \frac{e^{ikr}}{r} \int_0^a e' de' J_0(k e' \sin \theta)$$

$$= ik E_0 [\hat{n} \times \hat{y}] \frac{e^{ikr}}{r} \frac{1}{g^2} \int_0^{g^2} x J_0(x) dx$$

More identities

$$x J_0(x) = x J_1'(x) + J_1(x)$$

$$\int_0^{x_0} dx \underbrace{[x J_1' + J_1]}_{\text{parts}} = \int_0^{x_0} dx [-J_1 + J_1] + x_0 J_0(x)$$

$$\vec{E}(\vec{x}) = i k E_0 (\hat{n} \times \hat{y}) \frac{e^{i k r}}{r} a^2 \frac{J_1(\beta a)}{\beta a} \quad D-12$$

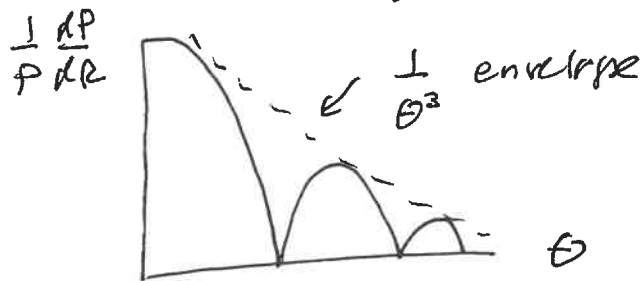
power $\propto |\vec{E}|^2$ incident flux $P_i = \frac{\epsilon}{8\pi} E_0^2 \times \pi a^2$

$$\frac{1}{P_i} \frac{dP}{d\Omega} \sim \frac{(ka)^2}{4\pi} \left[\frac{J_1(\beta a)}{\beta a} \right]^2 \times \text{polarization factors}$$

Diffraction minima at zeros of J_1 . First one's at $\beta a = 3.832 \approx ka\theta$.

\Rightarrow measure θ_1, θ_2 , know k , get a

$$\text{At large } x \quad \frac{J_1(x)}{x} \sim \sqrt{\frac{2}{\pi x^3}} \cos\left(x - \frac{3\pi}{4}\right)$$



Other ~~prints~~ prints discussed in Jackson

- Transmission coefficient $T = \int_{\text{Forward}} d\Omega \frac{1}{P} \frac{dP}{d\Omega}$

- $ka \ll 1$ or $\frac{a}{\lambda} \ll 1$ limit

- Scalar theory - basically the same result at small θ

$$\frac{1}{P} \frac{dP}{d\Omega} = (\text{our answer}) \times \begin{cases} 1 & \text{scalar} \\ 1 - \sin^2\theta \cos^2\varphi & \hat{E}_0 = \hat{y} \\ 1 - \sin^2\theta \sin^2\varphi & \hat{E}_0 = \hat{x} \end{cases}$$

Resolving power of optical instrument

Circular aperture, Fraunhofer limit

$$\vec{E}(x) = \frac{-ik}{2\pi} E_0 \frac{e^{ikr}}{r} [\hat{n} \times (\hat{z} \times \vec{E}_0)] \int_{\text{aperture}} dA' e^{i\vec{k} \cdot \vec{x}'} I$$

$$I = \int_{\text{aperture}} dA' e^{i(\vec{k}_0 - \vec{k}) \cdot \vec{x}'}$$

aperture in x-y plane

$$\int dA' = \int_0^a e' de' \int_0^{2\pi} d\phi'$$

~~Normal incidence: $\vec{x}' = (x', y', z')$~~ Circular aperture: $\vec{x}' = (e' \cos \phi', e' \sin \phi', 0)$ normal incidence $\vec{k}_0 = (0, 0, k_0) \Rightarrow \vec{k}_0 \cdot \vec{x}' = 0$

$$\vec{k} = k \left[\sin \theta \cos \phi, \sin \theta \sin \phi, \cos \theta \right]$$

~~Normal incidence?~~

Exercise in special functions (homework problem)

$$\frac{1}{P} \frac{dP}{d\Omega} \sim \frac{(ka)^2}{4\pi} \left[\frac{J_1(qa)}{qa} \right]^2 \times \text{polarization factors}$$

$$qa = ka \sin \theta \sim ka \theta$$

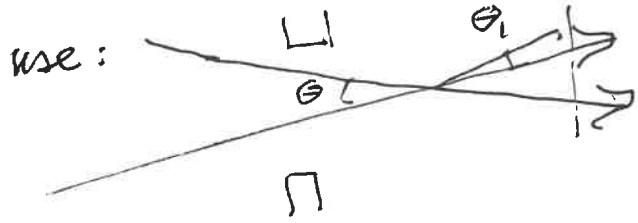


minima of $\frac{J_1(x)}{x}$ are $x = 1.22\pi, 2.33\pi, \dots$

(R-2)

$$x = kr\theta = \frac{2\pi a}{\lambda} \theta$$

first minimum $\theta_1 = 0.61 \frac{\lambda}{a}$



2 off set rays can be distinguished if $\theta > \theta_1$

→ Rayleigh criterion for resolving power of optical instrument, $\Delta\theta \sim 0.61 \frac{\lambda}{a} \approx 1.22 \frac{\lambda}{D}$

example: the eye, $\lambda \sim 5.6 \times 10^{-5}$ cm

• diameter of pupil 1.5 - 6 mm

$$5 \cdot 10^{-4} > \Delta\theta > 1 \times 10^{-4} \text{ radian}$$

1'34" to 0'24"

(Born + Wolfe)

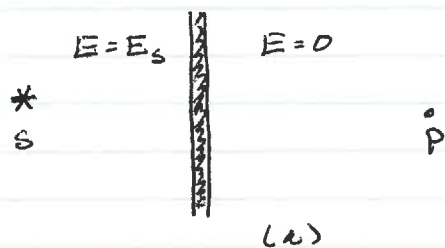
Babinet's Principle a la Feynman (VI:31-10)

Light comes through the holes in an opaque screen.

Similar problem

Replace holes by sources uniformly distributed over hole - so the diffracted wave is the same as though the hole were a new source. Strange: the hole is where there are no sources - not accelerating charges.

What is an opaque screen? "Opaque" - no field at P.

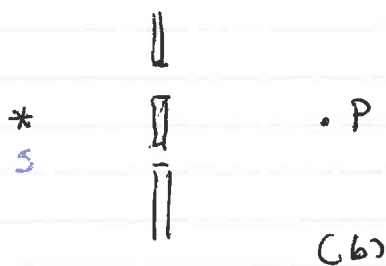


What is field at P? It is due to field of source E_s , plus fields from all the other charges around.

Charges in screen are set in motion by E_s , they must generate a field which exactly cancels E_s on back side of screen. (side toward observer) It's a miracle, this exact cancellation!

For if there weren't exact cancellation, the residual field would accelerate more charges in the screen, they would radiate - you would see something at P.

Now what about a wall with holes? Field at P = field due to S + field due to charges in walls.



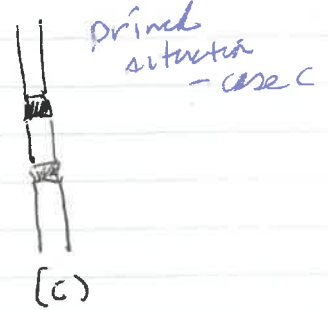
$$E_P = E_s + E_{\text{wall}}$$

~~Plugs up holes~~

Now plug up the holes with the same kind of material as the walls. (primed situation)

$$c) \quad E'_p = 0 = E_s + (E'_{wall} + E'_{plug})$$

$$E_p = (E_{wall} - E'_{wall}) - E'_{plug}$$



Now if the holes are not too small we'd expect (correction is from the edge of the holes) and in that case $E'_{wall} = E_{wall}$

$$E_p = -E'_{plug}$$

Field at P when there are holes in screen (case b)

$$= - (\text{Field produced by the parts of an opaque screen located ~~by~~ where the holes are})$$

It's an amazing forward backward argument -

~~that~~ arises because the source is cancelled by the motion of charges everywhere in the screen.