

## Set 12 – due 1 December

“The task is not to see what no one else has seen, but to think what no one else has thought, about that which everyone else has seen.” – Schrödinger

1) [20 points] Jackson 7.6 (a)–6, (b)–6, (c)–8.

2) [20 points] More about Jackson 7.2. You have already solved this problem to find the transmission and reflection coefficients. Now consider the case of an infinite planar dielectric medium of thickness  $d$  in the vacuum (i.e.  $n_3 = 1$  in 7.2). Assume that there is an incident electromagnetic wave of energy density  $u_0$  and frequency  $\omega$  directed normal to the surface of the plane, and compute the radiation pressure of the wave on the plane in two ways: (a) [7 points] Calculate the field momentum of the incident wave,  $p_i$ , the transmitted wave,  $p_t$ , and the reflected wave  $p_r$ . Then use momentum conservation to write  $\vec{p}_i = \vec{p}_t + \vec{p}_r$  + momentum of plate. (b) [7 points] Evaluate the stress tensor to the left and to the right of the slab. (c) [6 points] For what values of thickness  $d$  is the pressure a maximum?

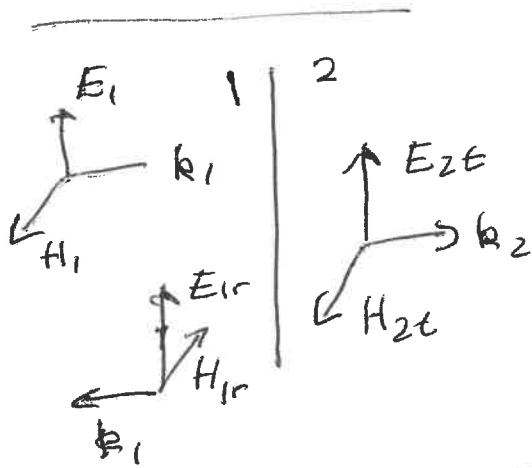
3) [10 points] Suppose that there is a magnetic field  $\vec{H}_0$  parallel to, and at the surface of, a good conductor. Beginning with the expressions for  $\vec{E}$  and  $\vec{H}$  in conductors (in Jackson Sec. 8.1), (a) [5 points] show that the time-averaged power loss into the conductor per unit area is

$$\frac{dP}{dA} = \frac{\mu_c \omega \delta}{4} |H_0|^2 = \frac{1}{2\sigma\delta} |H_0|^2. \quad (1)$$

(b) [5 points] What is the time-averaged magnetic energy density (energy per unit area) stored in the conductor, in terms of  $\vec{H}_0$ ?

The point of this problem is that this is how loss occurs for electromagnetic waves confined in a region with metallic boundaries: it is used to compute attenuation in a waveguide or the Q of a cavity.

7.6 - Radiation incident on an absorbing slab - 7.6.1  
 set  $\mu = \mu_0$  so that the index of refraction is  
 $n^2 = \epsilon / \epsilon_0$ . Choose coordinates so  $\vec{E} = \hat{x} E$ .



$$\text{Then } \vec{H} = \oint \mathbf{H} = \sqrt{\frac{\epsilon}{\mu}} \hat{n} \times \vec{E} \\ = \left( \frac{1}{\mu_0 c} n \right) \hat{n} \times \vec{E}.$$

$$n_1 = 1, \quad k_1 = \omega / c \equiv k$$

$$n_2 = n(\omega), \quad k_2 = n(\omega) k_1 = n(\omega) \frac{\omega}{c}.$$

In region 1  $E_{1x} = E_1 e^{i(kz - \omega t)} + E_{1r} e^{i(-kz - \omega t)}$

$$H_{1y} = \frac{1}{\mu_0 c} \left( E_1 e^{i(kz - \omega t)} - E_{1r} e^{i(-kz - \omega t)} \right)$$

In region 2  $E_{2x} = E_{2t} \exp[i(n(\omega) kz - \omega t)]$

$$H_{2y} = \frac{n(\omega)}{\mu_0 c} E_{2t} \exp[i(n(\omega) kz - \omega t)]$$

$E_x$  and  $H_{||}$  continuous at  $z = 0$ :  $E_1 + E_{1r} = E_{2t}$   
 $E_1 - E_{1r} = n(\omega) E_{2t}$

or  $\frac{E_{1r}}{E_1} = \frac{1 - n(\omega)}{1 + n(\omega)}$  and  $\frac{E_{2t}}{E_1} = \frac{2}{1 + n(\omega)}$

$$R = \left| \frac{1 - n(\omega)}{1 + n(\omega)} \right|^2 \quad ; \quad T = 1 - R = \frac{4 \operatorname{Re} n(\omega)}{|1 + n(\omega)|^2}$$

You can also get this directly from the Poynting vector:  $\langle \vec{S}_I \rangle = \frac{1}{2} \text{Re} (\vec{E}_I \times \vec{H}_I^*) = \frac{1}{2} \frac{1}{\mu_0 c} |\vec{E}_I|^2$

$$\langle \vec{S}_R \rangle = -\hat{z} \frac{1}{2} \frac{1}{\mu_0 c} |\vec{E}_{I,r}|^2$$

$$\langle \vec{S}_T \rangle = \frac{\hat{z}}{2 \mu_0 c} \text{Re} \left[ \frac{2}{1+n} \left( \frac{2n}{1+n} \right)^* \right] |\vec{E}_I|^2$$

(using  $\vec{H} \propto n(\omega) \vec{E}$ )

b) Eq. 6.134 gives the energy dissipated per unit time

$$W_{\text{loss}} = \text{Re} [2i\omega (W_E - W_M)] = \frac{1}{2} \text{Re} [i\omega (\vec{E} \cdot \vec{D}^* - \vec{B} \cdot \vec{H}^*)]$$

$$\vec{D} = \epsilon \vec{E} = \frac{n^2(\omega)}{\mu_0 c^2} \vec{E}, \quad \vec{B} = \mu_0 \vec{H}, \quad \vec{H} = \frac{n(\omega)}{\mu_0 c} \hat{n} \times \vec{E}$$

$$\text{so } W_{\text{loss}} = \frac{\omega}{2 \mu_0 c^2} \text{Im} \left\{ (n^2(\omega))^* - |n(\omega)|^2 \right\} |\vec{E}_2(x, z)|^2$$

In the  $\{ \}$  we need  $n^2 = (\text{Re } n + i \text{Im } n)^2$   
 $|n|^2 = (\text{Re } n)^2 + (\text{Im } n)^2$

$$\text{so } W_{\text{loss}} = \frac{\omega}{2 \mu_0 c^2} \left[ 2 \text{Re } n(\omega) - \text{Im } n(\omega) \right]$$

$$\times \frac{4}{|1-n(\omega)|^2} \exp \left[ -2 (\text{Im } n(\omega)) k z \right].$$

The energy loss per unit area is found by integrating

$W_{\text{loss}}$  over  $z$  going into region 2

$$\int_0^{\infty} dz W_{\text{loss}}(z) = \frac{\omega}{2 \mu_0 c^2} \cdot \frac{4}{|1+n(\omega)|^2} \frac{2 \text{Re } n - \text{Im } n}{2 \cdot \text{Im } n \cdot k} |\vec{E}_I|^2$$

and  $w = ck$  so this is

$$\frac{4 \operatorname{Re} n(\omega)}{|1+n(\omega)|^2} \frac{|E_i|^2}{2\mu_0 c^2} = T \cdot \langle S_i \rangle$$

The transmission coefficient times the incident flux.

c) Now we evaluate  $n^2 = 1 + \frac{i\sigma}{\omega\epsilon_0}$  in terms of skin depth  $\delta = \sqrt{\frac{2}{\mu_0 \omega}}$ . When  $\frac{\sigma}{\omega\epsilon_0}$  is large,

$$\begin{aligned} n(\omega) &\approx \sqrt{\frac{i\sigma}{\omega\epsilon_0}} = \frac{\sqrt{i\sigma\omega}}{\omega} \frac{1}{\sqrt{\epsilon_0}} \sqrt{\frac{\mu_0}{\mu_0}} = \frac{\sqrt{2i}}{\omega} \sqrt{\frac{\mu_0 \sigma \omega}{2}} \frac{1}{\sqrt{\mu_0 \epsilon_0}} \\ &= \sqrt{2i} \frac{c}{\omega \delta} \end{aligned}$$

$$\frac{1}{k} = \frac{c}{\omega} = \frac{\lambda}{2\pi} \equiv \bar{\lambda} \quad (\text{barred notation by analogy to } h = h/2\pi)$$

$$n(\omega) = \sqrt{2i} \frac{\bar{\lambda}}{\delta}$$

$$\text{And } i = e^{i\pi/2} \text{ so } \sqrt{2i} = \sqrt{2} \left( \cos \frac{\pi}{4} + i \sin \frac{\pi}{4} \right) = \sqrt{2} \left( \frac{1+i}{\sqrt{2}} \right)$$

or  $\sqrt{2i} = 1+i$  and

$$\operatorname{Re} n(\omega) = \operatorname{Im} n(\omega) = \frac{\bar{\lambda}}{\delta} \quad \text{Plug this into}$$

$$R = \left| \frac{1-n}{1+n} \right|^2 = \left| \frac{\sqrt{2i} \bar{\lambda} - \delta}{\sqrt{2i} \bar{\lambda} + \delta} \right|^2 = \left| \frac{1 - \frac{\delta}{\sqrt{2i} \bar{\lambda}}}{1 + \frac{\delta}{\sqrt{2i} \bar{\lambda}}} \right|^2$$

We are told that  $\delta/\bar{\lambda}$  is small, so just Taylor expand

$$R = 1 - \frac{4\delta}{\bar{\lambda}} \operatorname{Re} \frac{1}{\sqrt{2i}}$$

$$\sqrt{2i} = 1+i \text{ again so } \operatorname{Re} \frac{1}{\sqrt{2i}} = \operatorname{Re} \frac{1}{1+i} = \operatorname{Re} \frac{1-i}{2} = \frac{1}{2} \quad 7.6.4$$

$$R = 1 - \frac{2\delta}{\lambda}, \quad T = 1 - R = \frac{2\delta}{\lambda}$$

$$\text{Alternatively } T = \frac{4 \operatorname{Re}(\sqrt{2i} \lambda / \delta)}{|1 + \sqrt{2i} \lambda / \delta|^2} \approx \frac{4 \frac{\lambda}{\delta}}{2 \left(\frac{\lambda}{\delta}\right)^2} = \frac{2\delta}{\lambda}$$

Now return to p. 7.6.2,

$$W_{\text{loss}} = \frac{\omega}{2\mu_0 c^2} \frac{2 \operatorname{Re} n \cdot \operatorname{Im} n}{|1 + n(\omega)|^2} \cdot 4 |E_1|^2 \exp[-2 \operatorname{Im} n(\omega) k z]$$

$$= \frac{\omega}{2\mu_0 c^2} \frac{2 \left(\frac{\lambda}{\delta}\right)^2}{\left(1 + \frac{\lambda}{\delta}\right)^2 + \left(\frac{\lambda}{\delta}\right)^2} \cdot 4 |E_1|^2 \exp\left[-2 \frac{\lambda}{\delta} k z\right]$$

( $k = 1/\lambda$ )

$$\approx \frac{\omega}{2\mu_0 c^2} \cdot \frac{2 \left(\frac{\lambda}{\delta}\right)^2}{2 \left(\frac{\lambda}{\delta}\right)^2} \cdot 4 |E_1|^2 \exp\left(-\frac{2z}{\delta}\right)$$

This again uses  $\lambda/\delta \gg 1$  and  $k = 1/\lambda$ .

Again integrate over  $z$ : use  $w = c/\lambda$

$$W_{\text{loss}}^{\text{int}} = \int_0^\infty dz W_{\text{loss}}(z) = T \cdot \langle S_i \rangle = \frac{1}{2\mu_0 c^2} \frac{c}{\lambda} \cdot 4 \frac{\delta}{2} \times |E_1|^2$$

$$= \frac{\delta}{\mu_0 c \lambda} |E_1|^2$$

Ohmic loss is  $\frac{1}{2} \text{Re } \vec{J}_{2t}^* \cdot \vec{E}_{2t}$  and  $\vec{J} = \sigma \vec{E}$  so

$$\frac{\sigma}{2} |E_{2t}|^2 = \frac{\sigma}{2} \frac{4}{|n+1|^2} |E_1|^2 \exp\left(-\frac{2z}{\delta}\right)$$

$$= \left\{ \frac{\sigma}{2} \cdot \frac{4}{2\left(\frac{\pi}{\delta}\right)^2} \right\} |E_1|^2 \exp\left(-\frac{2z}{\delta}\right)$$

The prefactor in  $\{ \} = \frac{\sigma \delta^2}{\pi^2} = \frac{1}{\pi^2} \frac{2}{\mu_0 \omega}$

Integrate over  $z$  one last time

$$W_{\text{ohmic}}^{\text{int}} = \frac{2}{\mu_0 \omega} \frac{1}{\pi^2} \frac{\delta}{2} |E_1|^2 = \frac{1}{2\mu_0 \omega} \cdot \frac{2\delta}{\pi} |E_1|^2$$

substituting  $\omega = c/\lambda$ . This means that

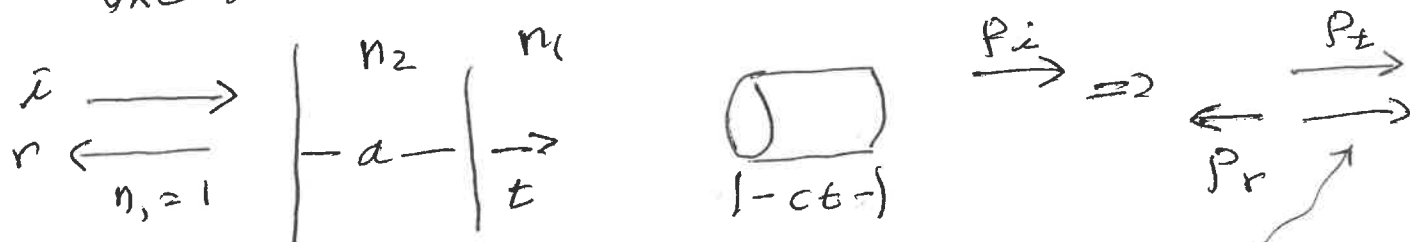
$$W_{\text{ohmic}}^{\text{int}} = W_{\text{loss}}^{\text{int}} = \langle S_i \rangle \cdot T = \frac{1}{2\mu_0 c} \frac{2\delta}{\pi} |E_1|^2$$

The point of this is that you can compute dissipation either via ohmic heating, or by using complex index of refraction, but not by doing both together - that is double counting. See the discussion in Jackson below Eq. 7.57.

2) More about 7.2. The time-averaged 7-2.1  
field momentum density is

$$\vec{g} = \frac{1}{2c^2} (\vec{E} \times \vec{H}^*)$$

The time averaged momentum transferred to a unit area surface on the boundary can be found by computing  $\vec{g}$  on both sides over a volume equal to  $V = \text{unit area} \times \text{thickness}$ , where thickness is equal to velocity ( $=c$ ) ~~times~~  $\times$  time. The pressure is the momentum absorbed by a unit area of the dielectric in a unit time



$$P_{\text{plate}} = P_i - P_t + P_r$$

$$\text{Pressure} = c \left[ \frac{1}{2c^2} \vec{E}_i \times \vec{H}_i^* \right] - c \left[ \frac{1}{2c^2} \vec{E}_r \times \vec{H}_r^* \right] - \frac{1}{c} \left[ \frac{1}{2c^2} \vec{E}_t \times \vec{H}_t^* \right]$$

$$= \frac{1}{2\mu_0 c^2} \left\{ |E_i|^2 + |E_r|^2 - |E_t|^2 \right\}$$

Using  $\frac{1}{\mu_0 \epsilon_0 c^2} = 1$ , the initial energy density is  $u_0$

$$u_0 = \frac{1}{4} \left[ \epsilon_0 |E_i|^2 + \frac{1}{\mu_0} |B_i|^2 \right] = \frac{\epsilon_0}{2} |E_i|^2$$

the pressure is  $u_0 \left[ 1 + \frac{|E_r|^2}{|E_i|^2} - \frac{|E_t|^2}{|E_i|^2} \right]$

$P = u_0 [1 + R - T]$ ; R and T are reflection & transmission coeffs.

We can simplify this using  $T+R=1$ , so

$1-T+R = 1-(1-R)+R = 2R$ . This makes sense - maximum pressure when  $\Rightarrow$  to a maximum

We now look at last ~~week's~~ week's solution, recall

$$r_{12} = \frac{n-1}{n+1} \equiv r \quad \text{and} \quad r_{23} = \frac{n_3-n_2}{n_3+n_2} \xrightarrow[n_2=n]{n_3=1} \frac{1-n}{1+n} = -r$$

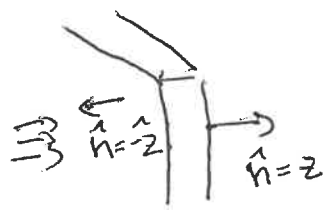
$$2R = \frac{2r^2 [1 - \cos d]}{1 - 2r^2 \cos d + r^4} \quad \text{where } d = 2k_2 d = \frac{2\omega_0}{c} n d.$$

b) Repeat with the stress tensor

$$\vec{T} = \frac{\epsilon_0}{2} \left[ \vec{E} \vec{E} + c^2 \vec{B} \vec{B} - \frac{1}{2} \mathbf{I} (|\vec{E}|^2 + c^2 |\vec{B}|^2) \right]$$

(replace  $\frac{1}{\mu_0}$  by  $\epsilon_0 c^2 \dots$ ). Integrate  $T$  over a surface of unit area on each side of the dielectric. At normal incidence, transversality says  $\hat{n} \cdot \vec{E} = \hat{n} \cdot \vec{B} = 0$  (for pressure into away from plate) so the first terms give nothing.

$$F_z = \int_{\text{on right}} T_{zz} n_z dA - \int_{\text{on left}} T_{zz} n_z dA \quad (\text{note - sign in } T!)$$



$$\frac{\text{Force}}{\text{area}} = \frac{1}{2\mu_0 c^2} \left[ -|E_x|^2 + |E_y|^2 + |E_z|^2 \right]$$

this is  $P \propto -T+I+R$  as we had before!



c) The pressure is proportional to 7.2.3

$1 - \cos 2k_2 d$  so we want  $\cos 2k_2 d = -1$   
For maximum pressure. This is

$$2k_2 d = (2n+1)\pi = \pi, 3\pi, 5\pi, \dots$$

$$k_2 = \frac{2\pi}{\lambda_2} = \frac{2\pi}{\lambda} \sqrt{\frac{\epsilon}{\epsilon_0}} \quad \text{where } \lambda_2 \text{ is the in-medium wavelength,}$$

$\lambda$  the wavelength in vacuum.

$$\text{Thus } d = \frac{(2n+1)\pi}{2k_2} = \frac{(2n+1)\pi}{2} \frac{\lambda_2}{2\pi} = \frac{2n+1}{4} \lambda_2.$$

The minimum  $d$  is  $\frac{\lambda_2}{4}$ .

It's a bit like last week, except then we wanted  $R=0$  for

$$n=1 \mid \sqrt{n} \mid n>1$$

while here we have

$$n=1 \mid n \mid n=1$$

$$R = \frac{4r^2}{(1+r^2)^2} \quad \text{at } \cos \alpha = -1, \quad r = \frac{n-1}{n+1}.$$

3) Inside a good conductor,

3.1

$$H = H_0 e^{-z/\delta} e^{i z/\delta}$$

where  $z$  is the normal distance into the conductor and  $\delta = \text{skin depth}$ . Jackson

Eq. 8.10 says

$$\vec{E} = \sqrt{\frac{\mu_0 \omega}{2\sigma}} (1-i) (\hat{n} \times H_0) \exp\left[-\frac{z}{\delta} + i\frac{z}{\delta}\right]$$

a) The power loss is

$$\frac{dP}{dA} = -\frac{1}{2} \text{Re } \hat{n} \cdot (E \times H^*) = \frac{1}{2} \sqrt{\frac{\mu_0 \omega}{2\sigma}} |H_0|^2$$

We introduce  $\delta^2 = \frac{2}{\mu_0 \omega \sigma}$  or  $\frac{1}{\sigma} = \frac{\delta^2 \mu_0 \omega}{2}$  so

the  $\sqrt{\quad}$  is  $\sqrt{\frac{\mu_0 \omega}{2} \delta^2 \frac{\mu_0 \omega}{2}}$  and

$$\frac{dP}{dA} = \frac{\mu_0 \omega \delta}{4} |H_0|^2 = \frac{\delta}{4} \frac{2}{\delta^2 \sigma} |H_0|^2 = \frac{1}{2\delta\sigma} |H_0|^2$$

b) The energy stored in a distance  $z$  in the metal is

$$U(z) = \frac{1}{4} \mu_0 |H(z)|^2 = \frac{\mu_0}{4} |H_0|^2 \exp\left[-\frac{2z}{\delta}\right].$$

The energy stored per unit area is  $\int_0^\infty U(z) dz$

so we integrate inward, the integral is

$$\frac{\mu_0}{4} \cdot \frac{\delta}{2} |H_0|^2 = \frac{\mu_0 \delta}{8} |H_0|^2.$$