

Vector and Scalar Potentials

$$\vec{J} \cdot \vec{B} = 0 \Rightarrow \vec{B} = \vec{\nabla} \times \vec{A}$$

$$\nabla \times \vec{E} + \frac{\partial \vec{B}}{\partial t} = 0 \Rightarrow \nabla \times \left(\vec{E} + \frac{\partial \vec{A}}{\partial t} \right) = 0$$

$$\Rightarrow \vec{E} + \frac{\partial \vec{A}}{\partial t} = -\nabla \Phi$$

or $\vec{B} = \vec{\nabla} \times \vec{A}, \vec{E} = -\vec{\nabla} \Phi - \frac{\partial \vec{A}}{\partial t}$

Gauge invariance: Maxwell's equations are invariant under the reparameterization (\equiv gauge transformation)

$$\vec{A}' = \vec{A}^* + \vec{\nabla} \chi$$

$$\Phi' = \Phi + \frac{\partial \chi}{\partial t}$$

[see Jackson & Okun
RMP 73 GE3 (2000)]

for any (differentiable) scalar function χ .

Proof: $\vec{B}' = \vec{\nabla} \times \vec{A}' = \vec{\nabla} \times \vec{A} = \vec{B}$

$$\vec{E}' = -\vec{\nabla} \Phi' - \frac{\partial \vec{A}'}{\partial t} = -\vec{\nabla} \Phi - \vec{\nabla} \frac{\partial \chi}{\partial t} - \frac{\partial \vec{A}}{\partial t} - \frac{\partial \vec{A}}{\partial t} \frac{\partial \chi}{\partial t}$$

What is the wave equation in terms of $\vec{\Phi}, \vec{A}$?

$$\vec{\nabla} \cdot \vec{E} = \frac{c}{\epsilon_0} = -\nabla^2 \Phi - \frac{\partial}{\partial t} (\vec{\nabla} \cdot \vec{A}) \quad (1)$$

$$\begin{aligned} \vec{\nabla} \times (\vec{\nabla} \times \vec{A}) &= \mu_0 \vec{J} + \frac{1}{c^2} \frac{\partial}{\partial t} \left(-\nabla \Phi - \frac{\partial \vec{A}}{\partial t} \right) \\ &= \nabla (\vec{\nabla} \cdot \vec{A}) - \nabla^2 \vec{A} = \\ &\quad \text{or } \nabla^2 \vec{A} = \frac{1}{c^2} \frac{\partial^2 \vec{A}}{\partial t^2} - \nabla \left(\vec{\nabla} \cdot \vec{A} + \frac{1}{c^2} \frac{\partial \vec{\Phi}}{\partial t} \right) = -\mu_0 \vec{J} \end{aligned} \quad (2)$$

Simplifying by making a gauge choice

What is the wave equation in terms of $\vec{\Phi}, \vec{A}$?

$$\nabla \cdot \vec{E} = \frac{c}{\epsilon_0} \Rightarrow \nabla \cdot \left\{ -\nabla \vec{\Phi} + \frac{\partial \vec{A}}{\partial t} \right\} = \frac{c}{\epsilon_0}$$

keep $\rightarrow -\nabla^2 \vec{\Phi} + \frac{\partial}{\partial t} (\nabla \cdot \vec{A}) = \frac{c}{\epsilon_0}$ (1)

$$\nabla \times (\vec{\nabla} \vec{\Phi}) = \mu_0 \vec{J} + \frac{1}{c^2} \frac{\partial \vec{E}}{\partial t}$$

$$\nabla \times (\nabla \times \vec{A}) = \mu_0 \vec{J} + \frac{1}{c^2} \frac{\partial}{\partial t} \left(-\nabla \vec{\Phi} + \frac{\partial \vec{A}}{\partial t} \right)$$

$$\nabla(\nabla \cdot \vec{A}) - \nabla^2 \vec{A} = \mu_0 \vec{J} - \frac{1}{c^2} \frac{\partial^2 \vec{A}}{\partial t^2} - \nabla \left(\frac{1}{c^2} \frac{\partial \vec{\Phi}}{\partial t} \right)$$

(2) $\nabla^2 \vec{A} - \frac{1}{c^2} \frac{\partial^2 \vec{A}}{\partial t^2} = -\mu_0 \vec{J} - \nabla \left(\nabla \cdot \vec{A} + \frac{1}{c^2} \frac{\partial \vec{\Phi}}{\partial t} \right)$

keep
hmm - not nice - but we have
the freedom to make a gauge choice

Lorentz gauge: $\nabla \cdot A + \frac{1}{c^2} \frac{\partial \Phi}{\partial t} = 0$

$$\left. \begin{aligned} 2) \quad \nabla^2 \vec{A} - \frac{1}{c^2} \frac{\partial^2 \vec{A}}{\partial t^2} &= -\mu_0 \vec{j} \\ 1) \quad \nabla^2 \Phi - \frac{1}{c^2} \frac{\partial^2 \Phi}{\partial t^2} &= -\frac{e}{G_0} \end{aligned} \right\} \text{Wave eqn again}$$

~~Btw, solutions of wave eqn in free space are waves~~

$$\text{In 1-d} \quad \left(\frac{d^2}{dx^2} - \frac{1}{c^2} \frac{d^2}{dt^2} \right) [f_1(x-ct) + f_2(x+ct)] = 0$$

"retarded" "advanced"

i.e. location of pulse $\Delta x = c\Delta t$

Suppose you have a $\vec{\Phi}$ and \vec{A} which do not satisfy

$\vec{\nabla} \cdot \vec{A} + \frac{1}{c^2} \frac{\partial \vec{\Phi}}{\partial t} = 0$. How to "gauge fix" to Lorentz gauge?

$$A' = A + \nabla X \Rightarrow \vec{\Phi}' = \vec{\Phi} - \frac{\partial X}{\partial t} \quad \text{Find } X \text{ so}$$

$$\nabla \cdot A' + \frac{1}{c^2} \frac{\partial \vec{\Phi}'}{\partial t} = 0 \Rightarrow \nabla^2 X - \frac{1}{c^2} \frac{\partial^2 X}{\partial t^2} + \underbrace{\nabla \cdot A + \frac{1}{c^2} \frac{\partial \vec{\Phi}}{\partial t}}_{=0}$$

i.e. $\nabla^2 X - \frac{1}{c^2} \frac{\partial^2 X}{\partial t^2} = -(\nabla \cdot A + \frac{1}{c^2} \frac{\partial \vec{\Phi}}{\partial t})$

X is solution of wave eqn w/ known source.

Also this says Lorentz gauge is not unique - if

$$\nabla^2 X - \frac{1}{c^2} \frac{\partial^2 X}{\partial t^2} = 0 \text{ then both } (\vec{A}, \vec{\Phi}) \text{ and } (\vec{A}', \vec{\Phi}')$$

in Lorentz gauge, solns of ¹wave eqn for same source.
homogeneous

Another useful gauge is $\left\{ \begin{array}{l} \text{Coulomb} \\ \text{radiation} \\ \text{transverse} \\ \text{physical} \end{array} \right\}$ gauge

$$\vec{\nabla} \cdot \vec{A} = 0$$

$$\text{In this gauge } \nabla^2 \Phi = C / \epsilon_0.$$

i.e. Instantaneous Coulomb potential

$$\Phi(x, t) = \frac{1}{4\pi\epsilon_0} \int d^3x' \frac{C(x', t)}{|x - x'|}$$

[keep this eqn] and $\nabla^2 \vec{A} - \frac{1}{c^2} \frac{\partial^2 \vec{A}}{\partial t^2} = \left\{ -\mu_0 \vec{J} + \frac{1}{c^2} \vec{\nabla} \frac{\partial \Phi}{\partial t} \right\}$

Wave eqn: $\vec{A}(r, -ct)$ but funny source

Let's break \vec{J} apart $\vec{J} = \vec{J}_T + \vec{J}_L$

Transverse current $\vec{\nabla} \cdot \vec{J}_T = 0$

Longitudinal current $\vec{\nabla} \times \vec{J}_L = 0$

Identity $\vec{\nabla} \times (\vec{\nabla} \times \vec{J}) = \vec{\nabla}(\vec{\nabla} \cdot \vec{J}) - \vec{\nabla}^2 \vec{J}$

or $\vec{\nabla}^2 \vec{J} = \vec{\nabla}(\vec{\nabla} \cdot \vec{J}) - \vec{\nabla} \times (\vec{\nabla} \times \vec{J})$

Now if $\vec{\nabla}^2 \vec{V} = -4\pi \vec{a}(x)$

$$\vec{V}(x) = \int \frac{a(x')}{|x - x'|} d^3x'$$

so (formally)

$$\vec{J}^{(0)} = -\frac{1}{4\pi} \int d^3x' \frac{\vec{\nabla}'(\vec{\nabla}' \cdot \vec{J})}{|x - x'|} + \frac{1}{4\pi} \int d^3x' \frac{(\vec{\nabla}' \times (\vec{\nabla}' \times \vec{J}))}{|x - x'|}$$

Now a parts integral and $\nabla' \frac{1}{|x-x'|} = -\nabla \frac{1}{|x-x'|}$

give

$$\vec{J}(x,t) = -\frac{1}{4\pi} \vec{\nabla} \int d^3x' \frac{\vec{\nabla}' \cdot \vec{J}}{|x-x'|} + \frac{1}{4\pi} \nabla_x \left(\nabla_x \int \frac{\vec{J}(x') d^3x'}{|x-x'|} \right)$$

The first term has no curl, it is J_L

The 2nd term has no divergence, it is J_T

Now in continuity equation $\nabla \cdot J = \frac{\partial e}{\partial t}$

This is J_L - only J_L particysaks in $\frac{\partial e}{\partial t}$

$$\text{Finally } \frac{1}{c^2} \vec{\nabla} \frac{\partial \Phi}{\partial t} = \frac{1}{c^2} \frac{1}{4\pi\epsilon_0} \vec{\nabla} \int d^3x' \frac{\frac{\partial e(x',t)}{\partial t}}{|x-x'|}$$

$$\frac{1}{\epsilon_0 c^2} = \mu_0 \text{ so this is } \mu_0 \vec{J}_L$$

$$\text{so } \vec{\nabla}^2 \vec{A} - \frac{1}{c^2} \frac{\partial^2 \vec{A}}{\partial t^2} = -\mu_0 [\vec{J} - \vec{J}_L] = -\mu_0 \vec{J}_T$$

\vec{A} is given by the transverse current. \vec{A} itself is transverse, $\vec{\nabla} \cdot \vec{A} = 0$ if $\vec{A} \sim e^{ik \cdot r}$, $\vec{\nabla} \cdot \vec{k} \cdot \vec{A} = 0$

$$\vec{A} \quad \vec{k}$$

In this gauge, electrodynamics consists of and in terms of potentials

- transverse radiation fields only from \vec{A}
- instantaneous Coulomb interaction

This is both useful and odd!

Useful: $\vec{\Phi} \sim \frac{1}{r}$, $\vec{E} \sim \frac{1}{r^2}$ from \vec{E} while
 $\vec{B} \sim \frac{1}{r^2}$ from \vec{B} while
radiation fields are \perp far away (still have
to show this): \vec{E}, \vec{B} only from \vec{A}, \vec{j}_t
 $\vec{A}, \vec{E} \& \vec{B}$ transverse

Furthermore, in the quantum theory of radiation
 \vec{A} is what becomes the photon field. 2 components
of \vec{A} . Happens, canonical momentum $p_{\text{cong}} \rightarrow$
 $\vec{A} \text{ is } \vec{E}$

$$H = E^2 + B^2 = E^2 + (k \times A)^2 \sim E^2 + k^2 A^2$$

$$\text{oscillator } H = p^2 + x^2$$

$$\text{oscillator} \rightarrow \sum_k \hbar \omega_k (n_k + \frac{1}{2}), n = \text{integer}$$

\Rightarrow photon! (No oscillator description of \vec{E})

Odd: Instantaneous Coulomb interaction. What
became of speed of light?
What happens to $\vec{j} \cdot \vec{A}$ under Lorentz transf.?

Also $\vec{j}_t = \vec{\nabla} \times \vec{\nabla} \times \int \frac{j(x') d^3x'}{|x-x'|}$

is not local in space, even if \vec{j} is local

Lorentz gauge also useful and odd:

Useful: single wave equation - everything
 (ϕ, \mathbf{A}) is causal, $\vec{\Phi}(\vec{r}-ct)$

Easy to keep track of Lorentz transformation
 properties

Odd = 3 A's, 1 ϕ : 4 ~~radiation~~ radiation potentials.
 How do you see light has 2 polarizations?

Can say several things to summarize

1) You can "pick a gauge" to simplify your problem.
 Sometimes can make a gauge choice with a tunable parameter in it. $\vec{A}(\vec{z}), \vec{\Phi}(\vec{z})$. At end (points venterine pattern, power radiated) should be no \vec{z} dependence. Useful to check calculations.

2) Something deep is going on in electrodynamics
 A peculiar reparameterization invariance which
 seems not to respect the fundamental degrees
 of freedom (2 A's vs 3 A's + $\vec{\Phi}$)

Could say: It's all $\vec{E} \leftrightarrow \vec{B}$, they are gauge inv.

But - Quantum mechanics involves \vec{A} ($\vec{P} \leftrightarrow \vec{e}\vec{A}$)
 interesting observed interference effects (Aharanov-Bohm)

- in Generalizations of E & M - electroweak, QCD
 not just $A, \vec{\Phi}$ are gauge dependent, so are $\vec{E} \leftrightarrow \vec{B}$.
 Only GI quantities are energy densities, Poynting vector,
 cross sections, etc.

See Jackson & Okun
RMP 77 663 (2001)

Field energy and momentum

Power = $\vec{F} \cdot \vec{v}$: rate E & B fields do work on point charge

$$\text{or } q\vec{v} \cdot \vec{E} = \sigma$$

1) gain of mechanical energy

2) rate of decrease of EM energy = $\frac{dE_{\text{mech}}}{dt} = \int_V \vec{J} \cdot \vec{E} d^3x$

3) rate fields do work on sources

Write RHS $\int_V \vec{J} \cdot \vec{E} d^3x = \int_V [\vec{\nabla} \times \vec{H} - \frac{\partial \vec{D}}{\partial t}] \cdot \vec{E} d^3x$

$$\nabla \times (\vec{E} \times \vec{H}) = \vec{H} \cdot (\vec{\nabla} \times \vec{E}) - \vec{E} \cdot (\vec{\nabla} \times \vec{H})$$

$$= -H \cdot \frac{\partial B}{\partial t} - E \cdot (\nabla \times H)$$

$$\int \vec{J} \cdot \vec{E} d^3x = - \int \left(\vec{J} \cdot (\vec{E} \times \vec{H}) + H \underbrace{\frac{\partial B}{\partial t}}_{+ E \frac{\partial D}{\partial t}} \right) d^3x$$

Assume linear medium - (Caution - this is a special case - dispersive systems with now) are different

$$\tau = -\frac{\partial}{\partial t} \left\{ \frac{1}{2} H \cdot B + \frac{1}{2} D \cdot E \right\} - \frac{\partial u}{\partial t} \quad n = \frac{\text{field energy}}{\text{density}}$$

$$\text{or } \tau = - \int \vec{J} \cdot \vec{E} d^3x = \int_V d^3x \left(\frac{\partial u}{\partial t} + \vec{\nabla} \cdot (\vec{E} \times \vec{H}) \right)$$

$$\text{or } \frac{\partial u}{\partial t} + \vec{J} \cdot \vec{E} = - \vec{\nabla} \cdot \vec{S}$$

$\vec{S} = \vec{E} \times \vec{H}$ = ~~propagating vector~~ = energy flux

$$= \frac{\text{energy}}{\text{area-time}}$$

$$\frac{d}{dt} (E_{\text{field}} + E_{\text{mech}} \text{ in } V) = - \int \vec{S} \cdot \hat{n} dA$$

= - rate of flow of energy
out of V

Momentum conservation uses $F = q(\vec{E} + \vec{v} \times \vec{B})$

$$\frac{d\vec{P}_{\text{mech}}}{dt} = \int_V d^3x [e\vec{E} + \vec{j} \times \vec{B}]$$

$$\vec{c} = \epsilon_0 \vec{\nabla} \cdot \vec{E} \quad \vec{j} = \frac{1}{\mu_0} \vec{\nabla} \times \vec{B} - \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

$$\vec{c} \cdot \vec{E} + \vec{j} \times \vec{B} = \epsilon_0 (\vec{\nabla} \cdot \vec{E}) \vec{E} + \epsilon_0 c^2 (\vec{\nabla} \times \vec{B}) \times \vec{B} - \epsilon_0 \frac{\partial \vec{E}}{\partial t} \times \vec{B}$$

$$\frac{\partial \vec{E}}{\partial t} \times \vec{B} = \frac{\partial}{\partial t} (\vec{E} \times \vec{B}) - \vec{E} \times \frac{\partial \vec{B}}{\partial t}$$

$$= \frac{\partial}{\partial t} (E \times B) - E \times (\vec{\nabla} \times \vec{E})$$

$$\vec{c} \cdot \vec{E} + \vec{j} \times \vec{B} = \epsilon_0 \left[\begin{array}{l} (a) E (\vec{\nabla} \cdot \vec{E}) + c^2 B (\vec{\nabla} \cdot \vec{B}) \\ - E \times (\vec{\nabla} \times \vec{E}) - c^2 B \times (\vec{\nabla} \times \vec{B}) \\ - \frac{1}{\epsilon_0} (E \times B) \end{array} \right]$$

zero, just to
be pretty

↙ LAS

$$\frac{d\vec{P}_{\text{mech}}}{dt} + \frac{d}{dt} \int_V \epsilon_0 (\vec{E} \times \vec{B}) d^3x = \int_S dA \hat{n} \cdot "momentum flow" \text{ into } V$$

2nd term is momentum in EM field

$$\begin{aligned} \vec{g} &= \epsilon_0 (\vec{E} \times \vec{B}) = \mu_0 \epsilon_0 (\vec{E} \times \vec{H}) = \frac{1}{c^2} (\vec{E} \times \vec{H}) \\ &= \frac{1}{c^2} \vec{S} \end{aligned}$$

The other terms - let's look at

$$[E (\vec{\nabla} \cdot \vec{E}) - E \times (\vec{\nabla} \times \vec{E})] \text{ direction}$$

$$\begin{aligned}
 &= E_1 \left(\frac{\partial E_1}{\partial x_1} + \frac{\partial E_2}{\partial x_2} + \frac{\partial E_3}{\partial x_3} \right) - E_2 \left(\frac{\partial E_2}{\partial x_1} - \frac{\partial E_1}{\partial x_2} \right) \\
 &\quad + E_3 \left(\frac{\partial E_1}{\partial x_3} - \frac{\partial E_3}{\partial x_1} \right) \\
 &= \frac{\partial}{\partial x_1} (E_1^2) + \frac{\partial}{\partial x_2} (E_1 E_2) + \frac{\partial}{\partial x_3} (E_1 E_3) \\
 &\quad - \frac{1}{2} \frac{\partial}{\partial x_1} (E_1^2 + E_2^2 + E_3^2)
 \end{aligned}$$

~~to~~ ~~the~~

$$G_0 []_{ij} := \sum_j \frac{\partial}{\partial x_j} G_0 (E_i E_j - \frac{1}{2} E^2 \delta_{ij})$$

a divergence! The object with 2 indices is
 a 2nd rank tensor, ~~the~~ called the
 Maxwell Stress Tensor "

$$\epsilon_0 []_i = \sum_j \frac{\partial}{\partial x_j} \epsilon_0 (E_i E_j - \frac{1}{2} E^2 \delta_{ij})$$

Divergence of a 2nd rank tensor, the "Maxwell stress tensor" → identical calculation for \vec{B}

$$T_{ij} = \epsilon_0 [E_i E_j + c^2 B_i B_j - \frac{1}{2} (E^2 + c^2 B^2) \delta_{ij}]$$

$$\frac{d}{dt} \left(\underset{in V}{\int} (P_{\text{mech}} + P_{\text{field}}) \right)_i = \sum_j \int d^3x \frac{\partial}{\partial x_j} T_{ij}$$

$$= \int_S dA \quad T_{ij} n_j \quad \rightarrow \hat{n} \text{ outward normal}$$

∴ Force per unit area ^{in direction i} transmitted across the surface, acting on particles & fields inside $V = T_{ii} n_i$
and increasing the momentum in $V =$

Recap Stress Tensor

$$\frac{d}{dt} (\vec{P}_{\text{mech}} + \vec{P}_{\text{fields}} \text{ in } V) = \int_S dA T_{ij} n_j \quad (1)$$

At

$$T_{ij} = \epsilon_0 \left[E_i E_j - \frac{1}{2} S_{ij} E^2 \right] + \frac{1}{\mu_0} \left[B_i B_j - \frac{1}{2} S_{ij} B^2 \right]$$

\downarrow 

T_{ij} = Pressure with component of force $\frac{\text{force}}{\text{unit area}}$ = pressure across a surface with normal \vec{n}

use Have objects in EM fields. Calculate forces acting on them by enclosing objects with boundary surface S . Add up total EM force on surface by integrating RHS of (1)

T_{ij} = symmetric rank-2 tensor a part of "energy-momentum tensor" = T^{mu} $mu = t, x, y, z$

Conservation of scalar quantity (charge) involves

4-vector (e, \vec{j}_0): $\frac{de}{dt} + \vec{\nabla} \cdot \vec{j} = 0$ $\Rightarrow \vec{j} \cdot \vec{n} = \vec{j}_0 \cdot \vec{n}$ = Flux of charge across surface

Conservation of vector quantity j^m needs another index, T^{mu} , $T_{ij} n_j = \text{flux of } j^m \text{ across}$

surface.

Pressure, etc for field variables?

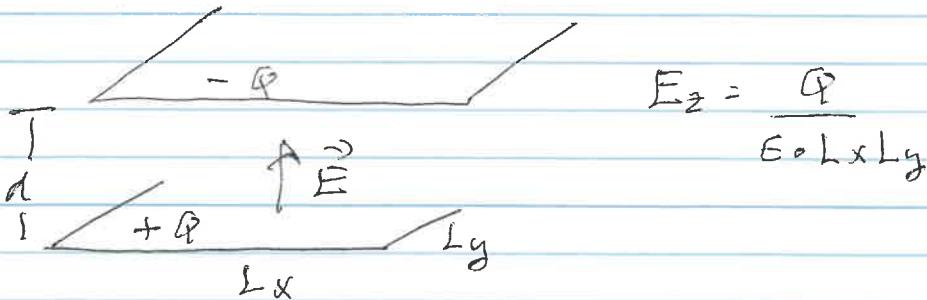
Example:

Stress tensor for constant $\vec{E} = \hat{z} E$ is

$$T = \frac{\epsilon_0}{2} \begin{bmatrix} -E^2 & 0 & 0 \\ 0 & -E^2 & 0 \\ 0 & 0 & E^2 \end{bmatrix} \quad T_{ij} = \epsilon_0 (E_i E_j - \frac{1}{2} \delta_{ij} E^2)$$

$$\int F_i dV = \text{inertial force in direction } i = \int dA T_{ij} n_j$$

Where did this E come from? a capacitor



$$E_z = \frac{Q}{\epsilon_0 L_x L_y}$$

- zz 1) plates attract each other - capacitor experiences negative pressure in z direction - we have to exert a force to hold them apart

- xx yy 2) charges on plates repel - plates want to fly apart, we have to exert a force to hold them together

Field energy $U = \frac{\epsilon_0}{2} E^2 \cancel{A} \times \cancel{d} \times \cancel{L_x L_y}$ where

$$U = \frac{1}{2\epsilon_0} \frac{Q^2 d}{L_x L_y} = \frac{\epsilon_0}{2} \left(\frac{Q}{\epsilon_0 L_x L_y} \right)^2 L_x L_y d$$

$$U = \frac{\epsilon_0}{2} \left(\frac{Q}{\epsilon_0 L_x L_y} \right)^2 L_x L_y d =$$

Force in z direction acts to decrease d

$$F_z = - \cancel{\frac{\partial U}{\partial d}} = - \frac{\epsilon_0}{2} E^2 \times \text{area}$$

$$= -T_{zz} \cdot \text{area}$$

~~pressure \rightarrow T_{zz}~~ Need outward pressure to hold plates apart (note $T_{zz} < 0$)

Force in x -direction acts to increase L_x

$$F_x = - \frac{\partial U}{\partial L_x} = - \frac{\partial}{\partial L_x} \left[\frac{Q^2 d}{2 \epsilon_0 L_x L_y} \right] = \frac{Q^2 d}{2 \epsilon_0 L_x^2 L_y}$$

Pressure = $\frac{F_x}{\text{area} = L_y d} = \frac{Q^2}{2 \epsilon_0 L_x^2 L_y} = \frac{\epsilon_0 E^2}{2} = -T_{xx}$



Need inward pressure to hold plates together (note $T_{xx} < 0$)

Alternative set of words for stress tensor

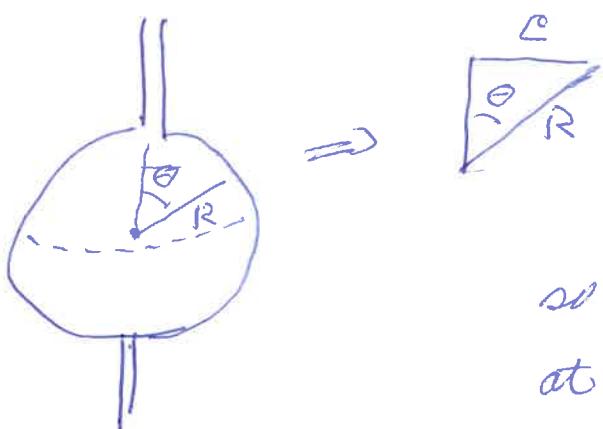
T_{ii} = pressure needed (from some non electromagnetic source)

in i th direction to maintain equilibrium

negative T : inward pressure needed

positive T : outward pressure needed

Comps 1991: A long conductor which is a thin cylindrical shell of radius "a" carries a current I into a thin conducting shell of radius $R \gg a$. The current flows uniformly through the shell. Cut the shell apart at the equator, hold it together, current continues to flow. What is the force required to pull the 2 halves apart?



\Rightarrow need \vec{B} : Ampere says

$$\oint \vec{B} \cdot d\ell = \mu_0 I_{\text{enc}}$$

so $\vec{B} = 0$ inside shell. Just outside,

$$\text{at } r = R \sin\theta, \quad 2\pi r B = \mu_0 I$$

or $\vec{B} = \frac{\mu_0 I}{2\pi r} \hat{\vec{r}} = \frac{\mu_0 I}{2\pi R \sin\theta} \hat{\vec{q}}$.

$$T_{ij} = \frac{1}{\mu_0} [B_i B_j - \frac{1}{2} \delta_{ij} B^2]$$

$$(\mu_0 \epsilon_0 = \frac{1}{c^2} \rightarrow \vec{E} = 0, \vec{B} = \text{constant})$$

Force / unit area in direction $\hat{\vec{z}}$ is ~~on~~ on surface w/outward normal \vec{n}_d is $= T_{ij} \vec{n}_d$.

Here we want $\hat{\vec{z}} = \hat{\vec{z}}$ (vertical), $\hat{\vec{n}} = \hat{\vec{r}}$ of the lower shell

$$\text{so we want } T_{zr} = \frac{1}{\mu_0} \left[\hat{z} \cdot \vec{B} B \cdot \hat{r} - \frac{1}{2} B^2 \hat{z} \cdot \hat{r} \right].$$

Integrate over the surface of the hemisphere

$$F_{z\theta\oplus} = -\frac{1}{2\mu_0} \hat{z} \cdot \hat{r} B^2 \text{ since } \vec{B} = \hat{r} B_0$$

Integrate over the surface of a hemisphere to find the total force

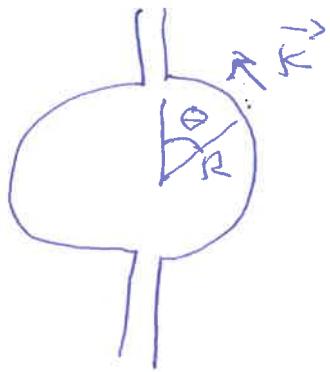
$$F_z = -\frac{1}{2\mu_0} \int_{\theta_0}^{\pi/2} 2\pi R^2 \sin\theta d\theta \left[\frac{\mu_0 I}{2\pi R \sin\theta} \right]^2 d\sin\theta$$

$$\theta_0 = \frac{a}{R}$$

$$= -\frac{\mu_0 I^2}{4\pi} \int_{\theta_0}^{\pi/2} \frac{\cos\theta}{\sin\theta} d\theta = -\frac{\mu_0 I^2}{4\pi} \ln \frac{1}{\sin\theta_0}$$

$$\approx -\frac{\mu_0 I^2}{4\pi} \ln \frac{R}{a} \quad - \text{the inward force holding the shell together.}$$

An alternate approach, not using the stress tensor - find the Lorentz force acting on the device via the surface current



$$F_z = \hat{z} \cdot \int dA \vec{K} \times \vec{B}$$

$$\vec{K} = -\hat{\theta} \frac{I}{2\pi R \sin \theta}$$

up!
circumference

$$F_z = 2\pi \int_{\theta_0}^{\pi/2} R^2 \sin \theta d\theta \left[\frac{I}{2\pi R \sin \theta} \right] \left[\frac{\mu_0 I}{2\pi R \sin \theta} \right]$$

$$\times \left[\hat{z} \cdot (-\hat{\theta} \times \hat{\phi}) \right]$$

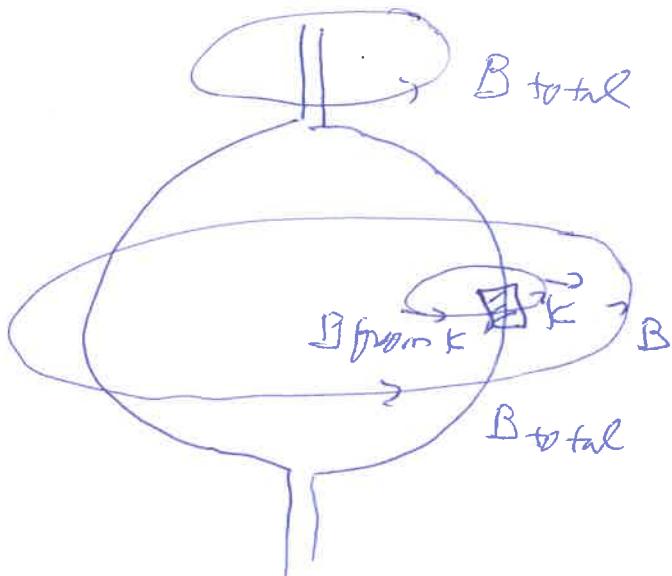
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$-\hat{\theta}$

$\hat{\theta} \times \hat{\phi}$ is radial

$$F_z = -\frac{2\mu_0 I^2}{4\pi} \int_{\theta_0}^{\pi/2} \frac{d\theta d\theta}{\sin \theta}$$

An extra 2! ~~Because~~ It's an overcount -
the B field has to come from all the currents
except the little piece of K we are integrating over



B_{front} extends inside the shell.

Outside:

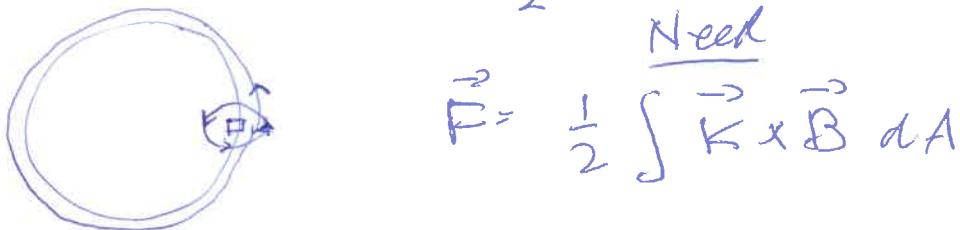
$$B_{DT} = B_{\text{outer}} + B_k = B$$

Inside \emptyset

$$\begin{aligned} B_{DT} &= 0 = B_{\text{outer}} - \cancel{B_k} \\ &= B_{\text{outer}} - B_k \\ &= B_{\text{outer}} - B_{\text{inner}} \end{aligned}$$

(W orientation)

$$\Rightarrow B_{\text{inner}} = \frac{B}{2} \quad (\approx B_k)$$



Summary: Stress tensor

advantage - very mechanical

disadvantage - unfamiliar

Direct - advantage - physical

disadvantage: 2's cross products

Maxwell Stress Tensor

The Maxwell stress tensor of the electromagnetic field has a form

$$\sigma_{\alpha\beta} = \frac{1}{4\pi} \left\{ E_\alpha E_\beta + H_\alpha H_\beta - \frac{1}{2} \delta_{\alpha\beta} (E^2 + H^2) \right\}. \quad (1)$$

Here α, β are spacial indices.

In particular, for a constant electric field directed along the z -axis, the stress tensor takes the form

$$\sigma = \frac{1}{8\pi} \begin{pmatrix} -E^2 & 0 & 0 \\ 0 & -E^2 & 0 \\ 0 & 0 & E^2 \end{pmatrix}. \quad (2)$$

Question: what is the meaning of the stress tensor? In particular, why is it that even though the field is along the z -axis, the stress tensor has components along x and y axes, of opposite sign to that along the z -axis.

The meaning of stress tensor, as discussed in elasticity theory, is the following. The integral over a closed surface gives the total force acting on this volume

$$\oint dn^\beta \sigma_{\alpha\beta} = \int dV F_\alpha, \quad (3)$$

where n^β is the vector normal to the surface and pointing in the outward direction.

In particular, the components $-\sigma_{\alpha\alpha}$ can be interpreted as pressure in the α -direction. The minus sign signifies the fact that, at positive pressure, we must apply the force "inward" to keep the material from expanding.

Going back to the electric field case, we recall that it is not just the stress tensor of the electric field which is conserved, but the total of the electric field and of the charges which created it. Thus, we have to consider the combined system of the charges and the electric field.

To create the constant electric field, we consider a capacitor, with large plates of lengths L_x and L_y , and the distance between the plates $d \ll L_x, L_y$, with the charge Q and $-Q$ on opposite plates. The electric field inside this capacitor is

$$E = \frac{4\pi Q}{L_x L_y}, \quad (4)$$

and it is pointed along the z -direction. It is clear that the opposite plates of the capacitor attract each other, in other words, the capacitor experiences negative pressure in the z -direction. It is also clear that the charges on a given plate of a capacitor repel each other. In other words, the capacitor should experience positive pressure in the x and y directions, or if the charges of the plates were simply floating in space, they would of course fly apart. This is the qualitative explanation of the form of the stress tensor (2).

To make the argument more quantitative, we calculate the attractive force between the plates. It's easiest to do by calculating the energy of the field

$$\mathcal{E} = \frac{E^2}{8\pi} L_x L_y d = \frac{2\pi d Q^2}{L_x L_y}. \quad (5)$$

The force in the z -direction is given by the derivative of the energy with respect to d , and the pressure is the force divided by the area, thus

$$p_z = \frac{\partial \mathcal{E}}{\partial d} \frac{1}{L_x L_y} = \frac{2\pi Q^2}{(L_x L_y)^2} = \sigma_{zz}. \quad (6)$$

At the same time, the force trying to tear the capacitor's plates apart is given by the derivative of \mathcal{E} with respect to L_x or L_y while the pressure is again obtained by dividing by the area ($d L_y$ in this case) and is given by

$$p_x = \frac{\partial \mathcal{E}}{\partial L_x} \frac{1}{L_y d} = -\frac{2\pi Q^2}{(L_x L_y)^2} = \sigma_{xx} \quad (7)$$

Harmonic fields, Lumped circuits

H-1

If everything has harmonic time dependence, we can write
 (for example) $\vec{E}(x, t) = \frac{1}{2} [\vec{E}_0(x) e^{-i\omega t} + \vec{E}_0^*(x) e^{i\omega t}]$
 $= \operatorname{Re} \vec{E}_0(x) e^{-i\omega t}$

where \vec{E}_0 is a complex vector. A dot product is

$$\vec{J} \cdot \vec{E} = \frac{1}{4} [\vec{J}_0 e^{-i\omega t} + \vec{J}_0^* e^{i\omega t}] \cdot [\vec{E}_0 e^{-i\omega t} + \vec{E}_0^* e^{i\omega t}] \\ = \frac{1}{4} \left[\vec{J}_0 \cdot \vec{E}_0 e^{2i\omega t} + \vec{J}_0^* \cdot \vec{E}_0 + \vec{E}_0^* \cdot \vec{J}_0 + \vec{J}_0^* \cdot \vec{E}_0^* e^{-2i\omega t} \right] \\ = \frac{1}{2} \operatorname{Re} [\vec{J}_0^* \cdot \vec{E}_0 + \vec{J}_0 \cdot \vec{E}_0 e^{-2i\omega t}]$$

Time average of $\vec{J} \cdot \vec{E} = \frac{1}{2} \operatorname{Re} \vec{J}_0^* \vec{E}_0$.

Convention is to work with complex fields, try to ignore $e^{i\omega t}$'s.

Maxwell's eqns: drop the " 0 " ~~overline~~, $\frac{\partial}{\partial t} = -i\omega$

$$\nabla \cdot \vec{D} = \rho \quad \nabla \cdot \vec{B} = 0 \quad \vec{\nabla} \times \vec{E} - i\omega \vec{B} \quad \vec{\nabla} \times \vec{H} = \vec{J} - i\omega \vec{D}$$

Power formula uses

$$\frac{1}{2} \int \vec{J}^* \cdot \vec{E} d^3x = \frac{1}{2} \int [\nabla \times \vec{H}^* - i\omega \vec{D}^*] \cdot \vec{E} d^3x$$

(repeat vector identities from before)

$$= -\frac{1}{2} \int \vec{\nabla} \cdot (\vec{E} \times \vec{H}^*) d^3x - i\omega \int d^3x \left[\frac{\vec{E} \cdot \vec{D}^*}{2} - \frac{\vec{B} \cdot \vec{H}^*}{2} \right]$$

\Rightarrow define complex Poynting vector $\vec{S} = \frac{1}{2} (\vec{E} \times \vec{H}^*)$

complex energy densities $W_e = \frac{1}{4} \vec{E} \cdot \vec{D}^*$

$$W_m = \frac{1}{4} \vec{B} \cdot \vec{H}^*$$

$$\text{Recap} \quad E(x, t) = \frac{1}{2} [E_0(x) e^{-i\omega t} + E_0(x)^* e^{i\omega t}]$$

~~$E(x, t) = \text{Re } E_0(x) e^{-i\omega t}$~~

$$J \cdot E = \frac{1}{2} \text{Re} [J_0^* E_0 + J_0 E_0^* e^{-2i\omega t}]$$

$$\text{Time average of } J \cdot E = \frac{1}{2} \text{Re } J_0^* E_0$$

energy loss power eqn

$$\frac{1}{2} \int_V \vec{J}^* \cdot \vec{E} d^3x + 2i\omega \int_V [W_E - W_M] d^3x = - \int \vec{S} \cdot \vec{n} dA$$

real part: time average energy conservation

imaginary part: "reactive energy" - stored, oscillating energy.

For linear medium, real ϵ, μ perfect conductors

$$\frac{1}{2} \operatorname{Re} \int \vec{J}^* \cdot \vec{E} d^3x = \operatorname{Re} \int \vec{S} \cdot \vec{n} dA = 0$$

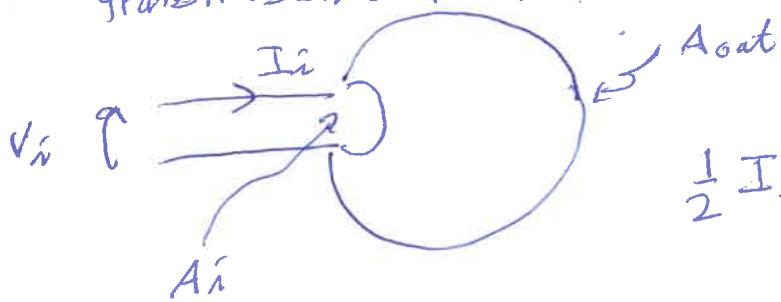
time avg power dissipated =

rate of doing work on ~~sources~~ = ~~rate of power flowing~~
sources in from outside

or ~~power generated~~ [energy flying out: $\int n > 0 ..$]

~~resistors~~ (resistivity: 2nd term has real part)

Circuit analogy: imagine radiation entering port or transmission line/coax



$$\frac{1}{2} I_i^* V_i = - \int_{A_i} \vec{S} \cdot \vec{n} dA$$

$$= \frac{1}{2} \int_V \vec{J}^* \cdot \vec{E} d^3x$$

$$+ 2i\omega \int_V d^3x (W_E - W_M)$$

$$+ \int_{A_{out}} \vec{S} \cdot \vec{n} dA$$

Complex Ohm's law $V_i = I_i Z$

$Z = R - i \bar{X}$ = impedance $(R + j\bar{X})$

$$\text{so } \frac{1}{2} I_i^* V_i = \frac{1}{2} |I_i|^2 Z$$

2 parts of Z . Real Z = resistance - energy loss.

Typically 2 kinds.

a) Ohmic resistance, $\vec{J} = \sigma \vec{E}$ - device gets warm!

$$R_\Omega = \frac{1}{|I_i|^2} \int \vec{J}^* \cdot \vec{E} d^3x = \frac{1}{|I_i|^2} \int_V \sigma |E|^2 d^3x$$

b) radiation resistance - energy goes out antenna

$$R_{rad} = \frac{1}{2 |I_i|^2} \int_{A_{out}} \vec{S} \cdot \vec{n} dA$$

~~both represent~~

$$\bar{X} = \text{"reactance"} = \frac{4\omega}{|I_i|^2} \int [W_m - W_E] d^3x = \bar{X}_L + \bar{X}_C$$

inductive & capacitive
reactance

$$W_m = \int W_m d^3x = \frac{1}{2} L |I|^2 \xrightarrow{\text{(real)}} \text{fine nec} = \frac{1}{4} L |I|^2$$

$$= \bar{X}_L \frac{|I_i|^2}{4\omega} : \bar{X}_L = \omega L$$

$$W_E = \int W_E d^3x = \frac{1}{2} \frac{Q^2}{C} \xrightarrow{\text{T.A.}} \frac{1}{4} \frac{|I_i|^2}{N^2 C} = -\bar{X}_E \frac{|I_i|^2}{4\omega}$$

$$\bar{X}_C = -\frac{1}{N^2 C}$$

(turn field energy into "EE" energy)

Circuit analogy often used. For us "radiation resistance" of antenna

$$\vec{J} = \sigma \vec{E}$$

$$\vec{B} = \mu \vec{H} \quad \dots$$

(phenomenological) relations between observables,
dynamical variables

$$W_{\text{mag}} = \frac{1}{2} \vec{B} \cdot \vec{H}$$

Can we imagine any arbitrary relation
between them ?
i.e. $\vec{J} = X \vec{B}$???

No. Such relations are constrained by
observation of "space-time symmetries"

rotational invariance

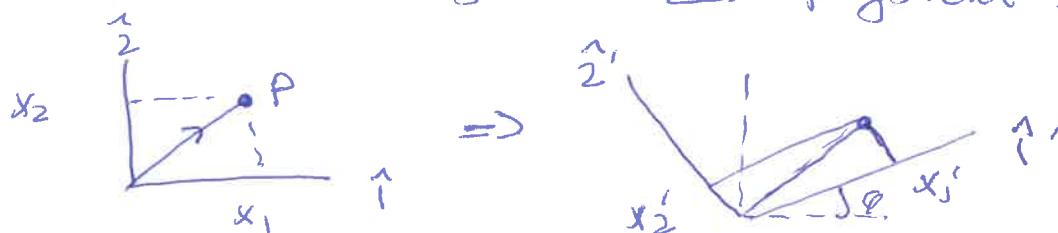
spatial inversion (parity)

time reversal symmetry

(Lorentz invariance - next semester!)

~~objects~~ We use objects which automatically encode
these symmetries.

- Rotations, first. I'll use a "passive picture"
- rotate coordinate system, not physical D, F



$$P = (x_1, x_2, x_3)$$

$$P = (x'_1, x'_2, x'_3)$$

$$x'_i = \sum_j a_{ij} x_j$$

For rotation about z-axis

$$a_{ij} = \begin{bmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\text{i.e. } x'_1 = x_1 \cos \theta + x_2 \sin \theta$$

$$x'_2 = -x_1 \sin \theta + x_2 \cos \theta$$

$$x'_3 = x_3$$

Length of vector is invariant: $\vec{x}' \cdot \vec{x}' = \vec{x} \cdot \vec{x}$

$$\sum_i x'_i x'_i = \sum_{ijk} a_{ij} a_{ik} x_j x_k$$

$$\text{or } \sum_i a_{ij} a_{ik} = \delta_{jk} \Rightarrow \underline{\underline{a}}^T \underline{\underline{a}} = \underline{\underline{I}}$$

$$\text{or. } = \sum_{ijk} a_{ij} a_{ik} \delta_{jk} = \delta_{jj}$$

i.e. orthogonal transformation

Note

i.e. orthogonal transformation

Note also $\det \mathbf{a} = 1$ for rotation (consider infinitesimal)

$$\begin{pmatrix} 1-\epsilon/2 & \epsilon & 0 \\ -\epsilon & 1-\epsilon^2/2 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Now consider objects with distinct properties under rotations:

a) Scalars: do not change under rotation

$$\text{ex. } \Phi(x) = \frac{g}{|x|} = \frac{g}{|\vec{x}'|} = \Phi(\vec{x}')$$

$$\text{or } \frac{g}{|x_1 - x_2|} = \frac{g}{|x'_1 - x'_2|}$$

[We have implicitly assumed g is a scalar!]

b) Vectors. Consider first \vec{x}

$$\text{transforms } \vec{x}' = \sum a_{ij} \vec{x}_j$$

i.e. components depend on rotation (on frame)
vector function

$$V_i'(\vec{x}') = \sum_j a_{ij} V_j(x_j) \text{ defines a vector}$$

$$\text{ex. } \vec{\nabla} \Phi = \left(\hat{x} \frac{\partial}{\partial x} + \hat{y} \frac{\partial}{\partial y} + \hat{z} \frac{\partial}{\partial z} \right) \frac{g}{|x|} = - \frac{g}{|x|^3} \vec{x} = \vec{E}$$

scalar vector

c) Tensor (rank 2 tensor) (written w.r.t. a cartesian tensor)

$$\text{defined by } T'_{ij} = \sum_{k \in} a_{ik} a_{jk} T_{kk} = \overset{\leftrightarrow}{T}$$

$$\text{Note } (\vec{A} \cdot \overset{\leftrightarrow}{T})_i = \sum_j A'_i T'_{ij} = \sum_i \sum_{k \in m} a_{ik} a_{jm} \overset{\leftrightarrow}{A}_k T_{nm}$$

$$= \sum_{k \in m} \delta_{kn} a_{jm} \overset{\leftrightarrow}{A}_k T_{nm} = \sum_m a_{jm} (\overset{\leftrightarrow}{A}_n T_{nm}) = \sum_m a_{jm} (\vec{A} \cdot \vec{T})_m$$

i.e. $\vec{A} \cdot \overset{\leftrightarrow}{T}$ transforms as a vector

Recap

Electrodynamics respects several space-time symmetries:

translational invariance

rotational invariance

spatial inversion (parity)

time reversal

To encode these symmetries in predictions, we work in terms of dynamical variables with simple transformation properties.

rotation: scalars $S' = S$
vectors

$$V'_i = \sum a_{ij} V_j$$

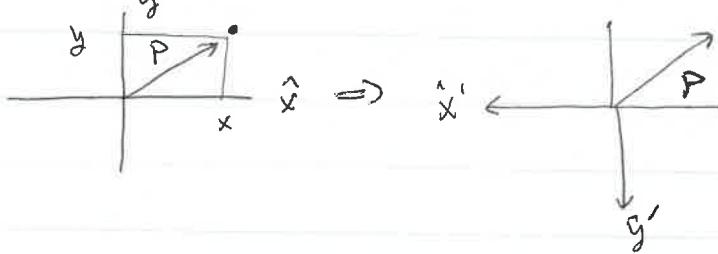
tensors

$$T'^{ij}_{kl} = \sum a_{ik} a_{jl} T_{kl}$$

$$\sum_i a_{ik} a_{il} = \delta_{kl}, \det a = 1$$

Next symmetry:

2) Spatial Inversion $\hat{x}' = -\hat{x}$, $\hat{y}' = -\hat{y}$, $\hat{z}' = -\hat{z}$



obviously $x' = -x$, $y' = -y$, $z' = -z$

$$\text{or } \vec{x}'_i = \sum_j a_{ij} x_j \quad \vec{a} = \begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

$$\vec{a}\vec{a}^T = 1$$

$$\det \vec{a} = -1$$

Contrast pure rotation: $\det \vec{a} = 1$

Inversion \neq rotation. Can combine the two into one axis.
Terminology: if $\det \vec{a} = 1$ "proper rotation"
if $\det \vec{a} = -1$ "improper rotation" =
proper rotation followed by
space inversion

Note $\sum_i x_i^2 = \sum_i x'_i^2$ in either case

a) Scalars: $\Phi(x') = \Phi(x)$; invariant under inversion

b) Polar vectors.

$$\vec{A}' = (A'_1, A'_2, A'_3) = - (A_1, A_2, A_3) = \underline{\underline{-A}}$$

bii) Axial vectors

$$\vec{A} = \vec{B} \times \vec{C} \quad A_i = \sum_k G_{ijk} B_j C_k$$

$$A'_i = \sum_k G_{ijk} (-B_j) (-C_k) = +A_i \quad \underline{\underline{=}}$$

a ii) Pseudoscalar - transforms as a scalar under proper rotations, flips sign under spatial inversion

ex. $\Psi^* = \vec{A} \cdot (\vec{B} \times \vec{C}) \quad A, B, C \text{ all polar vectors}$

$$\Psi' = A' \cdot (B' \times C') = -\Psi$$

3) Time Reversal. All the classical laws of physics
~~the laws of physics~~ are invariant to the sense of direction of time

time reversal is $dt \Rightarrow dt' = -dt$

$$\vec{F} = \frac{d\vec{p}}{dt} = -\vec{\nabla}u$$

$$\frac{d\vec{p}'}{dt'} = -\vec{\nabla}'u' = -\vec{\nabla}u \quad (\text{does not know anything about time})$$

$$\Rightarrow \vec{p}' = -\vec{p} \text{ under time reversal}$$

Makes sense, since $\vec{p} = m\vec{v} = m\frac{d\vec{x}}{dt}$

$$m\frac{d\vec{x}}{dt} \equiv -m\frac{d\vec{x}'}{dt'} \text{ under time reversal}$$

(here assume $d\vec{x} = d\vec{x}'$ does not know about time)

Classifying dynamical variables by
transformation properties under
coordinate changes

rotation

inversion (parity)

Scalar

rotation

inversion

$\xrightarrow{\text{SOS}}$ unchanged

$\xrightarrow{\text{SOS}}$ unchanged

Pseudoscalar

rotation $\xrightarrow{\text{P} \rightarrow \text{P}}$ unchanged

$\text{P} \rightarrow -\text{P}$

Polar Vector

$$V'_i = a_{is} V_s$$

$$\vec{V}' = -\vec{V}$$

Axial Vector

$$A'_i = a_{is} A_s$$

$$\vec{A}' = \vec{A}$$

Tensor

$$T'_{ij} = a_{ie} a_{ej} T_{em}$$

(after top of p. 4)

Now consider quantities encountered in electrodynamics

Kinematic quantity

$$\begin{aligned} m \\ \vec{r} \\ \vec{v} = \frac{d\vec{r}}{dt} \end{aligned}$$

$$\vec{p} = m\vec{v}$$

$$\vec{L} = \vec{r} \times \vec{p}$$

$$\vec{F} = \frac{d\vec{p}}{dt}$$

$$\vec{E} = \vec{v} \times \vec{F} = \frac{d\vec{L}}{dt}$$

$$T = p^2/2m$$

Rotation, Spatial inversion

scalar (e)

vector (o)

"

"

Axial vector (e)

vector (o)

Axial vector (e)

scalar (e)

Tire reversal
 $E = \text{even} = \text{no sign change}$

even

even

odd

"

"

"

"

"

Electromagnetic quantity

$$e$$

$$\vec{\Phi}$$

$$\vec{E} = -\nabla \vec{\Phi}$$

$$\vec{J} = e\vec{v}$$

$$\vec{A} = \mu_0 \int \vec{j} d^3x' / (x - x')$$

$$\vec{B} = \vec{\nabla} \times \vec{A}$$

$$\vec{H} = \frac{1}{\mu} \vec{B} \quad (\mu = \text{scalar})$$

$$\vec{S} = \vec{E} \times \vec{B}$$

$$\vec{T} \quad (\text{Maxwell stress tensor})$$

scalar (e)

"

vector (o)

"

"

axial vector (e)

"

vector (o)

"

2nd rank tensor

even (classical-
experimental fact -
charge is invariant
under Lorentz
transf.)
scalar under
rotation assumed
for spatial
inversion +
time reversal

Check consistency

$$1) \vec{\nabla} \cdot \vec{E} = 4\pi \frac{\rho}{\epsilon_0} : \text{contraction of vectors = scalar}$$

$$2) \vec{\nabla} \cdot \vec{B} = 0 \quad \text{spatial inv. odd} \times \text{even} = \text{odd but zero}$$

$$3) \vec{\nabla} \times \vec{E} = -\frac{1}{c^2} \frac{\partial \vec{B}}{\partial t} \quad V \times V = \text{axial vector}$$

$$\text{TR even} \times \text{even} = \text{even}$$

$$4) \vec{\nabla} \times \vec{B} = \mu_0 \vec{j} + \frac{1}{c^2} \frac{\partial \vec{E}}{\partial t}$$

The point of this exercise is that the laws of electrodynamics - the equations of electrodynamics should be consistent with respect to space-time symmetries - rotations, space inversion, time reversal. And we see they are.

Now take a step back. Suppose we know we have "physical" $\mathbf{D}, \mathbf{F}'s (E, B, \dots)$ but we don't know the equations. How can we constrain ~~more~~ more complicated quantities? Symmetries:

ex. EM energy. $U = \text{scalar}$, T even so

$$U(E, B) = c_1 E^2 + c_2 B^2 + \dots$$

no $E \cdot B$
but $(E \cdot B)^2$ etc

Suppose we imagine P for isotropic material is affected by E, B

P, E are polar vectors, T even
 B is axial vector T odd.

~~Consider~~ Note $\frac{\partial^n}{\partial t^n} (\vec{E} \times \vec{B})$ is polar
 T even if n is odd

$$\text{is } \frac{\partial^n}{\partial t^n} (\vec{E} \cdot \vec{B}^2) \quad n \text{ even}$$

$$\text{or } \frac{\partial^n}{\partial t^n} (\vec{E} \cdot \vec{B}) \vec{B} \quad n \text{ even}$$

$$\text{i.e. } \vec{P} = \chi_0 \vec{E} + \chi_1 \frac{\partial}{\partial t} (\vec{E} \times \vec{B}) + \chi_2 \frac{\partial^2}{\partial t^2} (\vec{E} \cdot \vec{B}^2) \\ + \chi_3 (\vec{E} \cdot \vec{B}) \vec{B} + \dots$$

L7

No story about χ 's (yet!)

but - missing term: No $P \propto \chi_B \vec{B}$

All front - why talk about it?

Immediate story - EM waves in
most complicated medium often
introduce phenomena (rigid)
relations. Are they "really true"
or is there a back story?