

# Magnetism

Historically, one could have introduced the magnetic field  $\vec{B}$  from

- the torque on a permanent magnetic dipole

$$\vec{\tau} = \vec{\mu} \times \vec{B}$$

- the force on a charged particle

$$\vec{F} = q \vec{v} \times \vec{B}$$

- the force on a segment of wire carrying a current  $I$

$$d\vec{F} = I d\vec{\ell} \times \vec{B}$$

Here current = charge going past, per unit time down the wire

More convenient for us is to define a current density

$\vec{J}$  = charge crossing unit area ~~per~~ per unit time

We assume conservation of charge, then

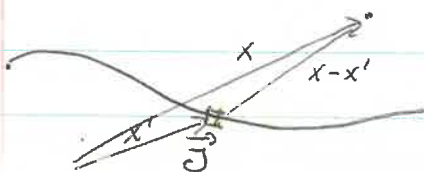
$$\frac{\partial \rho}{\partial t} + \nabla \cdot \vec{J} = 0$$

and magnetostatics is characterized by  $\frac{\partial \rho}{\partial t} = 0$ , so

$$\nabla \cdot \vec{J} = 0$$

Probably the best way to begin is with the Biot-Savart law

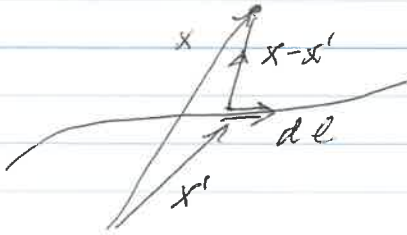
$$\vec{B}(\vec{x}) = \frac{\mu_0}{4\pi} \int d^3x' \vec{J}(\vec{x}') \times \frac{(\vec{x} - \vec{x}')}{|\vec{x} - \vec{x}'|^3}$$



$$\vec{J} = \frac{C \cdot m^{-1} \cdot s^{-1}}{m^2 \cdot sec} = \frac{C \cdot m^{-1} \cdot s^{-1}}{m^2} = \frac{C}{m^3} \cdot \frac{m}{sec}$$

= exorbity

or for wires 
$$d\vec{B}(x) = \frac{\mu_0 I}{4\pi} \oint \frac{d\vec{\ell} \times (\vec{x} - \vec{x}')}{|\vec{x} - \vec{x}'|^3}$$



We can "derive" Maxwell's differential equations from the Biot-Savart equation. Write it as

$$\vec{B}(x) = \frac{\mu_0}{4\pi} \vec{\nabla} \times \int \frac{\vec{J}(x') d^3x'}{|\vec{x} - \vec{x}'|}$$

Then  $\vec{\nabla} \cdot \vec{B} = 0$  immediately

$$\vec{\nabla} \times \vec{B} = \frac{\mu_0}{4\pi} \vec{\nabla} \times \vec{\nabla} \times \int \frac{\vec{J}(x') d^3x'}{|\vec{x} - \vec{x}'|}$$

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{V}) = \vec{\nabla} (\vec{\nabla} \cdot \vec{V}) - \nabla^2 \vec{V}$$

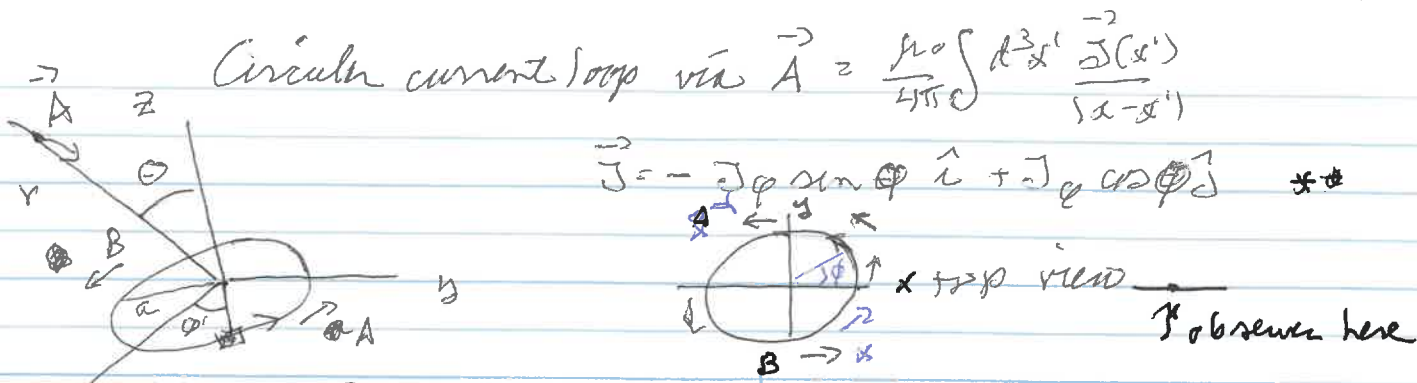
$$\text{so } \vec{\nabla} \times \vec{B} = \frac{\mu_0}{4\pi} \int d^3x' \left\{ \underbrace{\vec{\nabla} \left( \vec{J} \cdot \vec{\nabla} \frac{1}{|\vec{x} - \vec{x}'|} \right)}_{\text{part 1}} - \underbrace{\vec{J}(x') \nabla^2 \frac{1}{|\vec{x} - \vec{x}'|}}_{-4\pi \delta^3(\vec{x} - \vec{x}')} \right\} - \nabla_{x'} \frac{1}{|\vec{x} - \vec{x}'|}$$

$$\vec{\nabla} \times \vec{B} = -\frac{\mu_0}{4\pi} \underbrace{\vec{\nabla} \int d^3x' \vec{J}(x') \cdot \nabla_{x'} \frac{1}{|\vec{x} - \vec{x}'|}}_{\text{part 2}} + \mu_0 \vec{J}(x)$$

$$-\frac{\mu_0}{4\pi} \vec{\nabla} \int d^3x' \left( \underbrace{\vec{\nabla}_{x'} \cdot \vec{J}(x')}_{=0} \right) \frac{1}{|\vec{x} - \vec{x}'|} + \mu_0 \vec{J}(x)$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}(x)$$





Put observer in x-z plane. Then the x-components ~~A~~ cancel,  $A = A_y$  only.

By symmetry,  $A_y = A_\phi$  everywhere

pick  $x' = a [\sin\theta' \cos\phi', \sin\theta' \sin\phi', \cos\theta']$   
 $= a [\cos\phi', \sin\phi', 0]$   $\theta' = \pi/2$

~~total~~  $x = r [\sin\theta, 0, \cos\theta]$

keep only  $\vec{J}_y$

away from  $\theta'$

Jackson takes  $\vec{J} = \text{current/area} = \frac{I}{\pi a^2} \delta(r'-a) \delta(\cos\theta') \times \sin\theta'$

$\int \vec{J} = I \int \delta(r'-a) \delta(\cos\theta') \sin\theta' d\Omega'$

$\int \vec{J} = I \int \delta(r'-a) \delta(\cos\theta') \sin\theta' d\Omega'$  to force  $\vec{J}$  in x-y plane

$$A_\phi = \frac{\mu_0 I}{4\pi a} \int r'^2 dr' \delta(r'-a) \int d\Omega' \sin\theta' \delta(\cos\theta') \times \int \frac{d\phi' \cos\phi'}{|x-x'|}$$

$J_y$  \*\*  
(\*\*\*)

$$|x-x'|^2 = r^2 + a^2 - 2ra(\sin\theta \cos\phi')$$

$$A_\phi = \frac{\mu_0 I a}{4\pi} \int_0^{2\pi} \frac{\cos\phi' d\phi'}{[a^2 + r^2 - 2ar \sin\theta \cos\phi']^{1/2}}$$

Exact answer is an elliptic integral - not so useful!

Go to far field:  $\frac{1}{[a^2 + r^2 - 2ar \sin\theta \cos\phi']^{1/2}} = \frac{1}{r} + \frac{ar \sin\theta \cos\phi'}{r^3} + \dots$



$\psi_e'(\frac{\pi}{2}, 0) = 0$  if  $l$  is even, so we actually only have odd  $l$ .  
 Again, for away, keep  $l=1$ ,  $\psi_1' = \sqrt{\frac{3}{8\pi}} \sin\theta e^{i\phi}$

$$A_\phi = 2\pi \mu_0 I a \cdot \frac{a}{r^2} \cdot \frac{1}{3} \cdot \frac{3}{8\pi} \sin\theta = \frac{\mu_0}{4\pi} (\pi a^2 I) \frac{\sin\theta}{r^2}$$

The partial wave expansion has  $m \neq 0$  because the current goes around in a closed loop.

We can generalize to an arbitrary  $\mathbf{J}(\mathbf{x})$ . This will be the magnetic dipole term in a multipole expansion (higher orders get quite messy ---). Write

$$\frac{1}{|\mathbf{x}-\mathbf{x}'|} = \frac{1}{|\mathbf{x}|} + \frac{\mathbf{x} \cdot \mathbf{x}'}{|\mathbf{x}|^3} + \dots$$

$$A_i(\mathbf{x}) = \frac{\mu_0}{4\pi} \left[ \frac{1}{r} \int J_i(\mathbf{x}') d^3x' + \frac{x_{i\alpha}}{r^3} \int x'_{\alpha j} J_j(\mathbf{x}') d^3x' + \dots \right]$$

We must kill the first term. We know  $\nabla \cdot \mathbf{J} = 0$ ,  $\mathbf{J}$  is local.

Consider identity  $\int (f \vec{\mathbf{J}} \cdot \vec{\nabla}' g + g \vec{\mathbf{J}} \cdot \vec{\nabla}' f) d^3x' = 0$

Why - 2nd term -  $f \nabla' \cdot (g \vec{\mathbf{J}})$  parts

$$- f (g \nabla' \cdot \vec{\mathbf{J}} + \vec{\mathbf{J}} \cdot \nabla' g)$$

$$= \int (f \vec{\mathbf{J}} \cdot \nabla' g - f \vec{\mathbf{J}} \cdot \nabla' g) = 0$$

set  $f=1, g=x'_i$       $0 = \int [\vec{J} \cdot (\vec{\nabla}' x'_i) + x'_i \underbrace{\vec{J} \cdot \vec{\nabla}' 1}_0] d^3x'$

$0 = \int J_i(x'_i) d^3x'$      no just term in A eqn,  $\vec{\nabla}' x'_i = \hat{e}_i$

set  $f=x'_i, g=x'_j$      in  $f \vec{\nabla}' \cdot \vec{J}' g + g \vec{J}' \cdot \vec{\nabla}' f$

$\int (x'_i J'_j + x'_j J'_i) d^3x' = 0$      (\*)

so attach 2nd term in A eqn

~~$\sum_i x'_i \int J'_i d^3x'$~~       $\sum_j x'_j \int x'_i J'_i d^3x'$

$= -\frac{1}{2} \sum_j x'_j \int (x'_i J'_j - x'_j J'_i) d^3x'$      use \*

$= -\frac{1}{2} \sum_{j,k} x'_j \epsilon_{ijk} \int (\vec{x}' \times \vec{J})_k d^3x'$

$= -\frac{1}{2} (\vec{x} \times \int \vec{x}' \times \vec{J} d^3x')$

$= -\vec{x} \times \vec{m}$

Magnetic moment  $\vec{m} = \frac{1}{2} \int \vec{x}' \times \vec{J}(x') d^3x'$

so  $A(r) = \frac{\mu_0}{4\pi} \frac{\vec{m} \times \vec{r}}{r^3}$

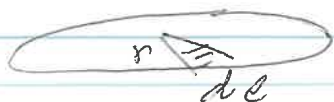
$\vec{B}(r) = \frac{\mu_0}{4\pi} \left[ \frac{3 \vec{r} (\vec{m} \cdot \vec{r}) - \vec{m} r^2}{r^5} \right]$

} dipole field

If current flows in a wire

$\vec{m} = \frac{I}{2} \int \vec{r} \times d\vec{\ell}$

If wire lies in plane  $\frac{1}{2} \vec{r} \times d\vec{\ell} = \text{area of triangle}$



$|\vec{m}| = I \cdot \text{area}$

$$A = \frac{\mu_0}{4\pi} \frac{m \times r}{r^3}$$

$$m = \int \frac{1}{2} d^3x (\vec{x} \times \vec{J}(\vec{x}))$$

M-8

Other simple magnetic moments are for rotating particles

$$\vec{J} = \sum_i q_i \vec{v}_i \delta(\vec{x} - \vec{x}_i)$$

$$m = \frac{1}{2} \sum_i q_i \vec{x}_i \times \vec{v}_i = \sum_i \frac{q_i}{2M_i} \vec{L}_i \quad L = r \times p$$

$$\left( \vec{m} = \frac{qL}{2Mc} \quad \text{in cgs} \right)$$

Spin:  $\vec{m} = \frac{g q \vec{S}}{2Mc}$   $\rightarrow g = 2$  for Dirac particle (electron)

And the formula for B isn't quite right, ~~it's~~

Here is an exact result,

$$\int_{\text{sphere of radius } R} \vec{B}(\vec{x}) d^3x = \frac{\mu_0}{4\pi} \cdot \frac{8\pi}{3} \vec{m}$$

To make our approximate formula agree with this, write it as

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \left[ \frac{3\vec{r}(\vec{m} \cdot \vec{r}) - \vec{m}r^2}{r^5} + \frac{8\pi}{3} \vec{m} \delta^3(\vec{r}) \right]$$

Complete dependence of B on an isolated dipole moment, treat dipole as point.

Let's show the identity

$$\begin{aligned} \int_{\text{sphere } r < R} \vec{B}(\vec{x}) d^3x &= \int_{r < R} \nabla \times \vec{A} d^3x = R^2 \int_{\text{surface } r=R} d\Omega \hat{n} \times \vec{A} \\ &= \int d\vec{A} (\hat{n} \times \vec{A}) \\ &= -R^2 \int d^3x' \vec{J}(\vec{x}') \times \int_{r=R} \frac{d\Omega \hat{n}}{|\vec{x} - \vec{x}'|} \quad \hat{n} \times \vec{A} = -(\vec{A} \times \hat{n}) \end{aligned}$$



$$A = \frac{\mu_0}{4\pi} \frac{\vec{m} \times \vec{r}}{r^3} \quad , \quad B = \nabla \times A$$

$$A_k = \frac{\mu_0}{4\pi} \epsilon_{k\ell m} \frac{m_\ell r_m}{r^3} \quad B_i = \epsilon_{ijk} \partial_j A_k$$

$$B_i = \frac{\mu_0}{4\pi} \epsilon_{ijk} \epsilon_{k\ell m} \partial_j \frac{m_\ell r_m}{r^3}$$

~~$\epsilon_{k\ell m} = \epsilon_{m\ell k}$~~  (cyclic)

$$B_i = \frac{\mu_0}{4\pi} \epsilon_{ijk} \epsilon_{k\ell m} \dots$$

$$\frac{\mu_0}{4\pi} (\delta_{i\ell} \delta_{jm} - \delta_{im} \delta_{j\ell}) \partial_j \frac{m_\ell r_m}{r^3}$$

$$= \frac{\mu_0}{4\pi} \left( \delta_{i\ell} \delta_{jm} - \delta_{im} \delta_{j\ell} \right) \left[ m_\ell \left( \frac{\delta_{jm}}{r^3} - \frac{3r_j r_m}{r^5} \right) \right]$$

$$= \frac{\mu_0}{4\pi} \left[ \begin{array}{cc} \text{Ia} & \text{Ib} \\ m_\ell \delta_{i\ell} \delta_{jm} \delta_{jm} & -3 r_j^2 m_i \\ \frac{m_i}{r^3} & + 3 r_i \left( \frac{m \cdot r}{r^5} \right) \end{array} \right]$$

$$B_i = \frac{\mu_0}{4\pi} \left[ 3 r_i \left( \frac{m \cdot r}{r^5} \right) - \frac{m_i}{r^3} \right] = \text{dipole}$$

Showing the identity

$$1) \int (\nabla \times \vec{A}) d^3x = \int d\vec{S}' \hat{n} \times \vec{A}$$

$$\text{Do it for a cube: } (\nabla \times \vec{A})_z = \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y}$$

$$(\vec{n} \times \vec{A})_z = n_x A_y - n_y A_x$$

$$\int dx dy dz \left[ \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right]$$

$$= \int dy dz [A_y(x_{\max}) - A_y(x_{\min})]$$

$$- \int dx dz [A_x(y_{\max}) - A_x(y_{\min})]$$

$$= \int d\vec{S}' [n_x (on \vec{S}') A_y - n_y (on \vec{S}') A_x]$$

$$\text{Then } \int_{\text{sphere } r < R} B(x) d^3x = \int_{r < R} (\nabla \times \vec{A}) d^3x = \int d\vec{S}' \hat{n} \times \vec{A}$$

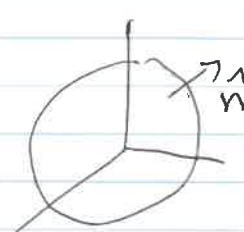
$$= R^2 \int_{\text{surface } r=R} d\Omega \hat{n} \times \vec{A}$$

$$\bullet \hat{n} \times \vec{A} = -\vec{A} \times \hat{n}$$

$$\int_{\text{sphere}} B(x) d^3x = -R^2 \int_{\text{sphere}} \vec{A}(x) \times \hat{n} d\Omega$$

$$\int B(x) d^3x = -R^2 \int d^3x' \vec{J}(x') \times \int_{r=R} d\Omega \frac{\hat{n}}{|\vec{x} - \vec{x}'|}$$

$$I = \int_{|x|=R} \frac{d\Omega \hat{n}}{|x-x'|} = \int_{|x|=R} d\Omega \cdot \hat{n} \frac{4\pi}{2e+1} \left[ \sum_{\substack{l \leq m \\ l > e+1}} \frac{r^l}{r^{e+1}} \frac{1}{2e+1} \frac{Y_l^m(x)}{Y_l^m(R)} \right]$$



$$\hat{n} = \hat{i} \sin\theta \cos\varphi + \hat{j} \sin\theta \sin\varphi + \hat{k} \cos\theta$$

$$= (\hat{i} + i\hat{j}) \sin\theta e^{i\varphi} + (\hat{i} - i\hat{j}) \sin\theta e^{-i\varphi} + \hat{k} \cos\theta$$

~~Each term of a~~ Each term of a  $\frac{1}{e=1}$  sum collapses! at  $r_>=r_>, r_<=r'$

$$I = \frac{4\pi}{3} \frac{r'}{r^2} \cdot \hat{n}' = \frac{4\pi}{3} \frac{\vec{x}'}{R^2}$$

$$\int \vec{B}(x) d^3x = -R^2 \int d^3x' \vec{\nabla} \cdot \vec{B}(x') \frac{4\pi}{3R^2} [\vec{\nabla}(x') \cdot \vec{x}']$$

$$= \frac{8\pi}{3} \cdot \frac{1}{2} \int d^3x' (\vec{x}' \cdot \vec{\nabla} B(x'))$$

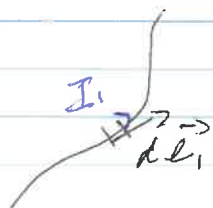
$$= \frac{8\pi}{3} \vec{m} \quad (!)$$

So far for exact result.

## Force and related quantities

Force on a current element due to  $\vec{B}$  is (if course)

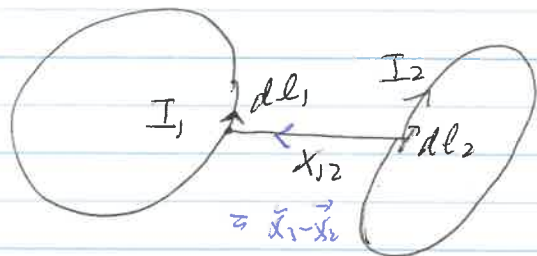
$$dF = I_1 d\vec{l}_1 \times \vec{B}$$



Suppose  $\vec{B}$  comes from another current loop -

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} I_2 \int \frac{d\vec{l}_2 \times (\vec{r} - \vec{r}_2)}{|\vec{r} - \vec{r}_2|^3}$$

so the force of loop #2 on loop #1 is



$$\vec{F}_{12} = \frac{\mu_0}{4\pi} I_1 I_2 \iint d\vec{l}_1 \times \left( \frac{d\vec{l}_2 \times \vec{x}_{12}}{|\vec{x}_{12}|^3} \right)$$

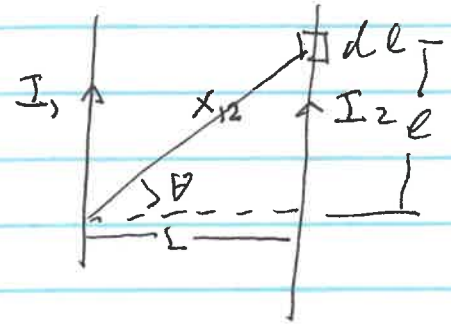
BAC-CAB rule  $d\vec{l}_1 \times (d\vec{l}_2 \times \vec{x}_{12}) = -(d\vec{l}_1 \cdot d\vec{l}_2) \vec{x}_{12} + d\vec{l}_2 (d\vec{l}_1 \cdot \vec{x}_{12})$

but  $\oint \frac{d\vec{l}_1 \cdot \vec{x}_{12}}{|\vec{x}_{12}|^3} = \oint d\vec{l}_1 \cdot \vec{\nabla} \frac{1}{|\vec{x}_{12}|} = 0$

2nd term gives,

$$\vec{F}_{12} = - \frac{\mu_0}{4\pi} I_1 I_2 \iint d\vec{l}_1 \cdot d\vec{l}_2 \frac{\vec{x}_{12}}{|\vec{x}_{12}|^3}$$

Easy example - two long straight wires



$$\frac{F}{\text{unit length}} = -\frac{\mu_0 I_1 I_2}{4\pi} \int \frac{dl}{x_{12}^2} \cdot \cos\theta$$

Project force transverse to line of current

$$\frac{L}{x_{12}} = \cos\theta \quad \frac{dl}{L} = \tan\theta$$

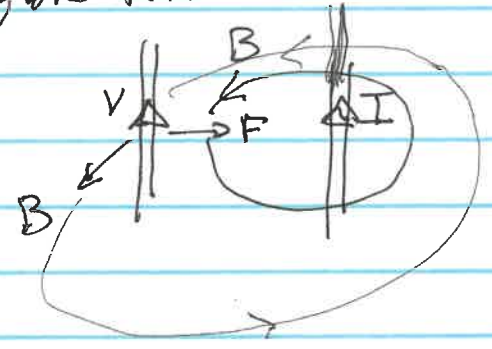
$$\frac{L}{x_{12}^2} = \frac{\cos^2\theta}{L^2} \quad dl = \frac{L}{\cos^2\theta} d\theta$$

$$\frac{F}{\text{length}} = -\frac{\mu_0 I_1 I_2}{4\pi} \int_{-\pi/2}^{\pi/2} \frac{\cos^2\theta}{L^2} \cdot \frac{L d\theta}{\cos^2\theta} \cdot \cos\theta$$

$$= -\frac{\mu_0}{4\pi} \frac{I_1 I_2}{L} \int_{-\pi/2}^{\pi/2} \cos\theta d\theta$$

$$= -2 \frac{\mu_0}{4\pi} \frac{I_1 I_2}{L}$$

attractive if currents flow in same direction  
(easy from RH rule)



$$\vec{v} \times \vec{B} = \vec{F}$$

A more general formula is

$$\vec{F} = \int \vec{J}(x) \times \vec{B}(x) d^3x$$

$$\vec{\tau} = \int [\vec{x} \times (\vec{J} \times \vec{B})] d^3x$$

Now assume the current is localized to a small region near the origin, Taylor expand  $\vec{B}$

$$B_k(x) = B_k(0) + \vec{x} \cdot \vec{\nabla} B_k(0) + \dots$$

$$F_i = \epsilon_{ijk} \left[ B_k(0) \underbrace{\int J_j(x) d^3x}_{\text{zero}} + \int J_j(x) \vec{x} \cdot \vec{\nabla} B_k(0) d^3x + \dots \right]$$

Do a parts  $\int$  on 2nd term a la magnetic dipole derivation

$$\vec{y} = \vec{\nabla} B_k(0) \text{ is outside the } J,$$

2nd term is  $\vec{y} \cdot \int \vec{x} J_j(x) d^3x = -\frac{1}{2} \left[ \vec{y} \times \left[ \int \vec{x} \times \vec{J}_j(x) d^3x \right] \right]_j$   
 $= (\vec{m} \times \vec{y})_j$  where  $\vec{m} = \text{magnetic moment}$

$$F_i = \epsilon_{ijk} (\vec{m} \times \vec{\nabla})_j B_k(0) = \cancel{(\vec{m} \times \vec{\nabla}) \cdot \vec{B}}$$

$$\vec{F} = (\vec{m} \times \vec{\nabla}) \times \vec{B}(0)$$

$$= \vec{\nabla} (\vec{m} \cdot \vec{B}) - \vec{m} (\vec{\nabla} \cdot \vec{B})$$

$$= -\vec{\nabla} [-\vec{m} \cdot \vec{B}]$$

$$\circ \circ \quad U = -\vec{m} \cdot \vec{B}(0)$$

also  $\vec{\tau} = \vec{m} \times \vec{B}(0)$

For 2 dipoles

$$U(m_1, m_2) = -\frac{\mu_0}{4\pi} \left[ \frac{3(\vec{m}_1 \cdot \vec{r})(\vec{m}_2 \cdot \vec{r}) - m_1 m_2 r^2}{r^5} + \frac{8\pi}{3} \vec{m}_1 \cdot \vec{m}_2 \delta(\vec{r}) \right]$$

## Macroscopic Equations, again

Let's begin with  $\vec{\nabla} \cdot \vec{B} = 0$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}_{\text{total}}$$

and introduce  $\vec{B} = \mu_0 (\vec{H} + \vec{M})$

with

$$\vec{\nabla} \times \vec{H} = \vec{J}_{\text{macro}}$$

so 
$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}_{\text{macro}} + \mu_0 \vec{\nabla} \times \vec{M}$$

i.e. the magnetization contributes to  $\vec{B}$  like a current density, the "magnetization current density"

$$\vec{J}_M = \vec{\nabla} \times \vec{M}$$

We also need a "constitutive relation" between  $\vec{B}$  &  $\vec{H}$ . For many materials it's linear

$$\vec{B} = \mu \vec{H} \quad \mu = \text{permeability}$$

$\mu / \mu_0 \equiv \text{rel. permeability}$

although in general, life gets complicated, especially for ferromagnetics

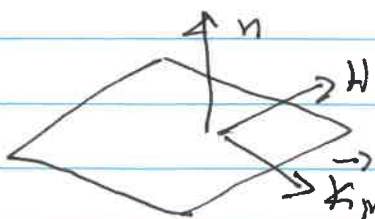
Boundary conditions for  $\vec{B}$  &  $\vec{H}$  at interfaces are easy!



$$\vec{\nabla} \cdot \vec{B} = 0 \Rightarrow \vec{B}_1 \cdot \vec{n} = \vec{B}_2 \cdot \vec{n}$$

$$\vec{\nabla} \times \vec{H} = \vec{J}$$

$$\vec{n} \times (\vec{H}_2 - \vec{H}_1) = \vec{K}$$



$\vec{K}_{\text{macro}}$  - surface current density

$$\left[ \begin{array}{l} \mu_2 \vec{K} = 0 \text{ (H-free)} \\ \text{continuous} \end{array} \right]$$

# Boundary Value Problems in Magnetostatics M-11

The generic situation is  $\nabla \cdot \vec{B} = 0$ ,  $\nabla \times \vec{H} = \vec{J}_{\text{macro}}$

Plus given  $\vec{B} = \vec{B}(\vec{H})$  or  $\vec{B} = \mu_0(\vec{H} + \vec{M})$

with  $\vec{B} \cdot \hat{n}$  continuous

$$\hat{n} \times \Delta \vec{H}_{\text{tan}} = \vec{K}_{\text{tan}} \quad \text{at interfaces}$$

2 text book cases:

a) linear permeability:  $\vec{B} = \mu \vec{H}$

b) specified  $\vec{M}$

If  $\vec{B} = \mu \vec{H}$   $\mu = \text{const}$  can try using  $\vec{A}$  s.t.  $\vec{B} = \nabla \times \vec{A}$

$$\nabla \times \vec{H} = \nabla \times \left( \frac{1}{\mu} \nabla \times \vec{A} \right) = \vec{J}$$

$$\nabla \times \nabla \times \vec{A} = \mu \vec{J}$$

$$\nabla(\nabla \cdot \vec{A}) - \nabla^2 \vec{A} = \mu \vec{J}$$

and in Coulomb gauge  $\nabla \cdot \vec{A} = 0$

$$\nabla^2 \vec{A} = -\mu \vec{J} \quad (\text{as before})$$

"Hard Ferromagnet":  $\vec{M}$  given,  $\vec{J} = 0$  has several possibilities, built on  $\nabla \times \vec{H} = 0$

1)  $\vec{B} = \mu_0(\vec{H} + \vec{M}) \rightarrow \nabla \times \vec{B} = \mu_0 \nabla \times \vec{M} \equiv \mu_0 \vec{J}_M$

Volume magnetization current density

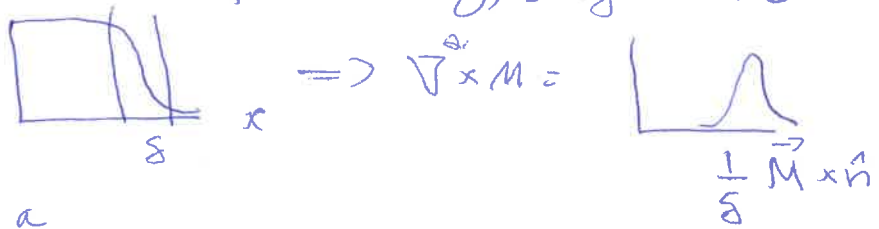
$$\vec{J}_M = \nabla \times \vec{M}$$



With no boundaries

$$\vec{A}(x) = \frac{\mu_0}{4\pi} \int d^3x' \frac{\vec{\nabla}' \times \vec{M}(x')}{|x-x'|}$$

If  $M$  has a sharp boundary, you can



separate off a

surface magnetic current density

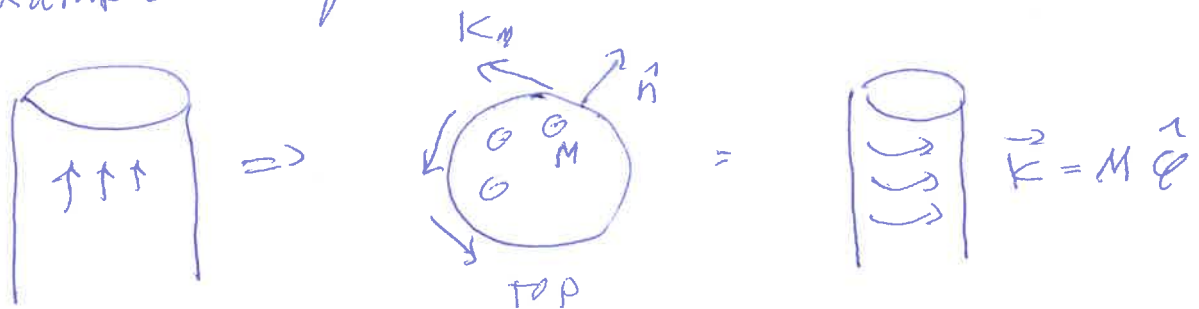
$$K_M(x') = \vec{M}(x') \times \hat{n}'$$

~~$A(x) = \frac{\mu_0}{4\pi} \int d^3x'$~~   $\int d^3x \rightarrow \int \delta dA$   $\text{cancels } \frac{1}{\delta}$

$$\vec{A}(x) = \frac{\mu_0}{4\pi} \int_V d^3x' \frac{\vec{\nabla}' \times \vec{M}(x')}{|x-x'|} + \frac{\mu_0}{4\pi} \int \frac{(\vec{M}(x') \times \hat{n}')}{|x-x'|} dA$$

(curl - don't overcount!)

example: uniform magnet,  $M$  constant inside



This is the familiar analog of the bar magnet and the solenoid: can do a direct attack

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{K}_M$$

bar magnet  $\rightarrow$  solenoid  $\rightarrow$  Biot-Savart or Ampere

# Magnetic Scalar Potential

M-13

$$\text{If } \vec{J}_{\text{macro}} = 0 \text{ then } \vec{\nabla} \times \vec{H} = 0$$

$$\text{so we can write } H = -\vec{\nabla} \Phi_M$$

$\Phi_M \equiv$  "magnetic scalar potential"

$$\text{ex. 1 } \vec{B} = \mu H, \mu = \text{constant},$$

$$\nabla \cdot B = 0 \Rightarrow \nabla^2 \Phi_M = 0$$

$$\text{ex. 2 } \vec{B} = \mu_0 \vec{H} + \vec{M}, \nabla \cdot B = 0 \text{ is}$$

$$\nabla \cdot H = -\nabla \cdot M$$

$$\nabla^2 \Phi_M = -c_M$$

$$c_M = -\vec{\nabla} \cdot \vec{M} \text{ (magnetic pole density!)} \\ \text{volume}$$

$$\Phi_M(x) = -\frac{1}{4\pi} \int d^3x' \frac{\vec{\nabla}' \cdot \vec{M}(x')}{|x-x'|}$$

example: suppose  $M$  is smooth, do a parts

$$\Phi_M = +\frac{1}{4\pi} \int \vec{M}(x') \cdot \vec{\nabla}' \frac{1}{|x-x'|}$$

$$\text{then } \vec{\nabla}' \frac{1}{|x-x'|} = -\vec{\nabla} \frac{1}{|x-x'|}$$

$$\Phi_M = -\frac{1}{4\pi} \vec{\nabla} \cdot \int \frac{\vec{M}(x')}{|x-x'|} d^3x'$$

$$\text{Far away, } \frac{1}{|x-x'|} \sim \frac{1}{r}$$

$$\begin{aligned}\Phi_M(\vec{x}) &\sim -\frac{1}{4\pi} \left( \vec{\nabla} \frac{1}{r} \right) \cdot \int d^3x' \vec{M}(x') \\ &= \frac{m \cdot \hat{r}}{4\pi r^3}\end{aligned}$$

This is the usual dipole formula for a scalar potential, with  $\vec{m} = \int d^3x' \vec{M}(x')$

With a sharp boundary for  $M$  we can treat it as discontinuous. Then - just as for a dielectric we have a volume pole density

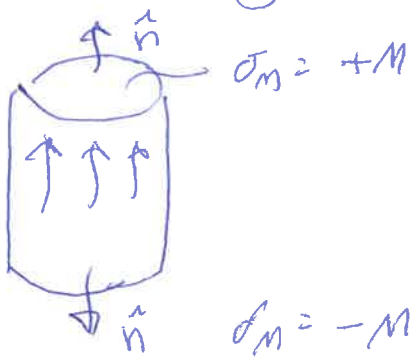
$$\rho_M = -\vec{\nabla} \cdot \vec{M}$$

and a surface pole density

$$\sigma_M = \hat{n} \cdot \vec{M}$$

$$\Phi_M(x) = \frac{1}{4\pi} \int_V \frac{\rho_M(x')}{|x-x'|} d^3x' + \frac{1}{4\pi} \int \frac{\sigma_M(x')}{|\vec{x}-\vec{x}'|} dA'$$

Bar magnet again - with constant  $M$



$$\nabla^2 \Phi = \begin{array}{l} \text{diagonal lines} + \\ \text{diagonal lines} - \end{array}$$

(contrast w/  $\vec{C}_M = \vec{M} \times \hat{n}$ !)



## Magnetized Sphere

Uniformly magnetized sphere of radius "a"

$$\vec{M} = \hat{z} M_0 \quad 0 < r < a$$

(not true for other shapes)

answer: it's a pure dipole. Many ways to solvea)  $\Phi_M$ ; use surface  $\sigma_M = \hat{n} \cdot \vec{M} = M_0 \cos \theta$ 

$$\int \frac{\sigma_M(x') d^2x'}{4\pi|x-x'|} = \Phi_M(r, \theta) = \frac{M_0 a^2}{4\pi} \int d\Omega' \cos \theta' \frac{1}{|x-x'|}$$

 $\cos \theta'$ : Legendre expansion only has  $l=1$ !

$$\Phi_M = \frac{1}{3} M_0 a^2 \frac{r < a}{r^2} \cos \theta \quad \frac{2}{3} \cdot \frac{2\pi}{4\pi}$$

$$\text{Inside, } \Phi_M = \frac{1}{3} M_0 r \cos \theta = \frac{1}{3} M_0 z$$

$$\vec{H} = -\nabla \Phi_M \Rightarrow H_z = -\frac{1}{3} M_0$$

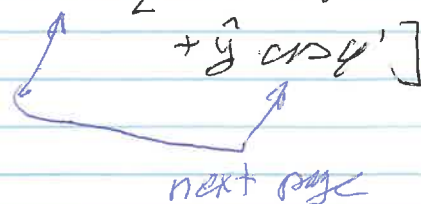
$$\vec{B} = \mu_0 [\vec{H} + \vec{M}] = +\frac{2}{3} \mu_0 M_0 \hat{z}$$

Outside, a pure dipole,  $\vec{m} = \frac{4\pi}{3} a^3 \vec{M} = \text{dipole moment}$ 

$$\text{b) } \vec{J}_M = 0, \quad \vec{K}_m = \vec{M} \times \hat{n} = M_0 \sin \theta \hat{e}_\phi$$

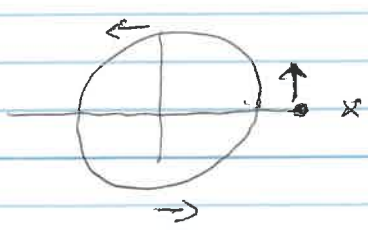


$$\vec{A}(x) = \hat{\phi} A_\phi(x) = \frac{\mu_0 M_0 a^2}{4\pi} \int d\Omega' \sin \theta'$$

Integrate current loop,  $\vec{K} = M_0 \sin \theta' [-\hat{x} \sin \phi' + \hat{y} \cos \phi']$ 

At  $\varphi=0$   $\vec{A}(x) = A_\varphi(x) = \frac{\mu_0 M_0 a^2}{4\pi} \int d\Omega' \frac{\sin\theta' \cos\varphi'}{|\vec{x}-\vec{x}'|}$

$= A_\varphi \hat{y}$



(recall cancellation of x-currents)

$\sin\theta' \cos\varphi' = -\sqrt{\frac{8\pi}{3}} R_{1,1} \Rightarrow l=1, m=1$   
in harmonic expansion

$A_\varphi = \frac{\mu_0}{4\pi} \left(\frac{4\pi}{3}\right) M_0 a^2 \frac{r < \sin\theta}{r^2}$

have to check carefully! dipole again - just have to recognize it.

~~$\sqrt{\frac{8\pi}{3}} [Y_{1,1} + Y_{1,-1}]$~~

~~$= \sqrt{\frac{8\pi}{3}} \sqrt{\frac{3}{8\pi}} \times 2$~~

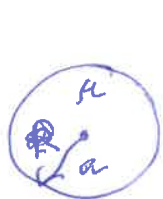
# Permeable sphere in external B-field

We've seen the math before!

In each region

$$\vec{J} = 0, \quad \vec{\nabla} \times \vec{H} = 0$$

$$\vec{B} \propto \vec{H} \quad (\vec{B} = \mu \vec{H} \text{ or } \mu_0 \vec{H})$$



$$\mu_0 \vec{B} \rightarrow \vec{B}$$

$$\text{and } \nabla \cdot \vec{B} = 0 \rightarrow$$

$$\nabla^2 \Phi_M = 0, \quad \vec{H} = -\nabla \Phi_M$$

$$\text{so } \Phi_M^{\text{out}} = \left[ -\frac{B_0}{\mu_0} r + \frac{C}{r^2} \right] \cos \theta \quad \text{Call } (A \text{ or } B)$$

$$\Phi_M^{\text{in}} = D r \cos \theta$$

all other partial waves vanish - then

$$1) \text{ Match } \Phi_M: \quad D \cdot a = -\frac{B_0 a}{\mu_0} + \frac{C}{a^2} \rightarrow \frac{C}{a^3} = D + \frac{B_0}{\mu_0}$$

$$2) \text{ match } \vec{B} \cdot \hat{n}: \quad \mu \frac{\partial \Phi_M^{\text{in}}}{\partial r} = \mu_0 \frac{\partial \Phi_M^{\text{out}}}{\partial r} \quad \text{at } r=a,$$

$$\mu D = -B_0 + 2\mu_0 \frac{C}{a^3}$$

$$\mu D = -B_0 - 2\mu_0 \left[ D + \frac{B_0}{\mu_0} \right]$$

$$(\mu + 2\mu_0) D = 3B_0 \Rightarrow D = \frac{3B_0}{\mu + 2\mu_0}$$

$$\text{so inside the sphere } \Phi_M = \frac{3B_0}{\mu + 2\mu_0} r \cos \theta = \frac{3B_0}{\mu + 2\mu_0} z$$

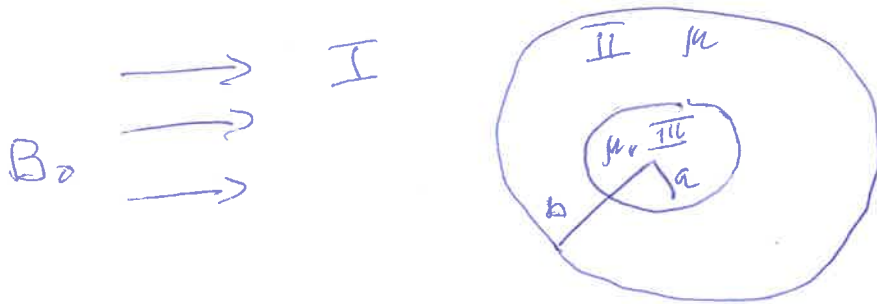
$$\vec{H} = \hat{z} \cdot \frac{3B_0}{\mu + 2\mu_0} \quad \vec{B} = \frac{\vec{B}}{\mu} \quad \text{and } \vec{B} = \mu_0 (\vec{H} + \vec{M}) \Rightarrow \vec{M} = \frac{\vec{B}}{\mu_0} - \vec{H}$$

$$\vec{M} = \hat{z} \cdot \frac{3B_0}{\mu + 2\mu_0} \left[ \frac{\mu}{\mu_0} - 1 \right] = \hat{z} \cdot \frac{3}{\mu_0} \left[ \frac{\mu - \mu_0}{\mu + 2\mu_0} \right] B_0$$

similar to  $\vec{P}$  for dielectric sphere

# Magnetic Shielding

MS-1



Want  $\Phi_M$  on the interior of the sphere  
 Yet again only  $l=1$ .

$$\Phi_I = \frac{1}{\mu_0} \left[ -B_0 r + \frac{E b^3}{r^2} \right] \cos \theta$$

$$\Phi_{II} = \frac{1}{\mu} \left[ B r + \frac{C b^3}{r^2} \right] \cos \theta$$

$$\Phi_{III} = \frac{1}{\mu_0} D r \cos \theta$$

coefficients chosen with malice!

$H_t$  or  $\Phi$

$B_r$  ( $B = \mu H$ )

$$\frac{1}{\mu_0} [-B_0 + E] = \frac{1}{\mu} (B + C)$$

$$\frac{1}{\mu} \left[ B + C \frac{b^3}{a^3} \right] = \frac{1}{\mu_0} D$$

$$B_0 + 2E = -B + 2C$$

$$-B + 2C \frac{b^3}{a^3} = -D$$

or

$$\begin{pmatrix} 1 & -\frac{\mu_0}{\mu} & -\frac{\mu_0}{\mu} & 0 \\ -2 & -1 & 2 & 0 \\ 0 & 1 & \frac{b^3}{a^3} & -\frac{\mu}{\mu_0} \\ 0 & -1 & 2 \frac{b^3}{a^3} & 1 \end{pmatrix} \begin{pmatrix} E \\ B \\ C \\ D \end{pmatrix} = \begin{pmatrix} B_0 \\ B_0 \\ 0 \\ 0 \end{pmatrix}$$

4 equations, 4 unknowns - ~~awful!~~ awful! but

intensity case is  $\mu \gg \mu_0$  - easy to get  $\mu$

$\frac{\mu}{\mu_0} \sim rD^{3-6}$ . Then easy to get an approximate solution:

1) top line:  $E = B_0$ . Then

$$\begin{bmatrix} -1 & 2 & 0 \\ 1 & r & -\hat{\mu} \\ -1 & 2r & 1 \end{bmatrix} \begin{matrix} B \\ C \\ D \end{matrix} = \begin{pmatrix} 3B_0 \\ 0 \\ 0 \end{pmatrix}$$

$$\text{setting } \hat{\mu} = \frac{\mu}{\mu_0} \quad r = \frac{b^3}{a^3}$$

$$\text{top line: } \cancel{3B_0} - B + 2C = 3B_0$$

$$B = -3B_0 + 2C$$

$$\text{2nd line: } -3B_0 + (r+2)C - \hat{\mu}D = 0$$

$$\text{3rd line: } 3B_0 + (2r-2)C + D = 0$$

$$\text{or } \left[ (r+2)C - \hat{\mu}D = 3B_0 \right] \frac{1}{r+2}$$

$$\left[ -(2r-2)C - D = 3B_0 \right] \frac{1}{2r-2}$$

$$\left[ \frac{-\mu}{r+2} \cdot -\frac{1}{2r-2} \right] D = \cancel{3B_0} \left( \frac{1}{r+2} + \frac{1}{2r-2} \right)$$

$$\frac{-\mu(2r-2) - (r+2)}{(r+2)(2r-2)} D = 3B_0 \frac{-3r}{(r+2)(2r-2)}$$

~~keep  $\hat{\mu}$~~



$$D = \frac{-9 \cdot B_0 \cdot r}{\dots}$$

$$\dots + 2\hat{\mu}(r-1) + (r+2)$$

drop the  $r+2$  '6'  $\hat{\mu} = \frac{\mu}{\mu_0} \gg 1$

$$r = \left(\frac{b}{a}\right)^3$$

$$\text{If } b = a + \delta \quad r = \left(1 + \frac{\delta}{a}\right)^3 = 1 + \frac{3\delta}{a}$$

$$D \approx \frac{-9B_0}{6 \left[ \frac{\mu}{\mu_0} \right] \left( \frac{\delta}{a} \right)}$$

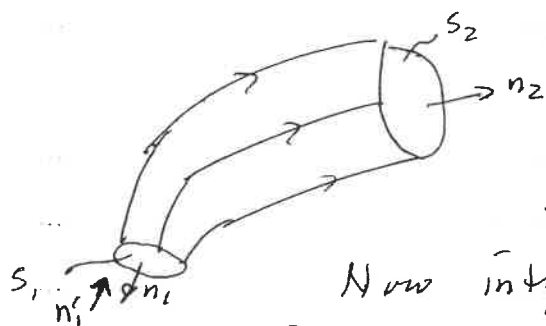
you win with big  $\frac{\mu}{\mu_0}$

lose with thin shell!

There are some useful approximations for dealing with the fields from permanent magnets. Let's begin by imagining a region of space filled with magnetic field and construct "magnetic field lines" - lines whose direction shows the direction of  $\vec{B}$  at a point. Now imagine a tube of flux, a volume

bounded on its side by lines of  $B$  but not cut by them.

The surface areas at the ends of the tube are  $S_1$  and  $S_2$ .



Now integrate  $\nabla \cdot \vec{B}$  over the tube

$$\int_V \nabla \cdot \vec{B} \, dV = 0 = \int_{S_2} \vec{B} \cdot \hat{n} \, dA - \int_{S_1} \vec{B} \cdot \hat{n}' \, dA$$

$$= \Phi(S_2) - \Phi(S_1)$$

$\Phi$  = magnetic flux - i.e. flux lines are conserved.  
(by ~~construction~~ construction)

This is not true for  $H$ :

$$\int_{S_1} \vec{H} \cdot \hat{n} \, dA - \int_{S_2} \vec{H} \cdot \hat{n}' \, dA = - \int_V \nabla \cdot \vec{H} \, dV$$

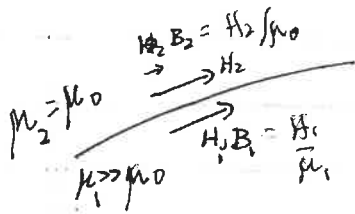
$$= \int_V \rho_m \, dV$$

= total magnetic pole strength intercepted by the flux tube.

Now if we have a magnet or a permeable material with a large  $\mu$ ,  $B$  is (mostly) confined to the magnet, except at the poles. Why? because  $H_{\pm}$  is continuous

field lines -  
lines tangent  
to mag  
field

at the side



so  $H_1 = H_2$

but  $B = \mu H$

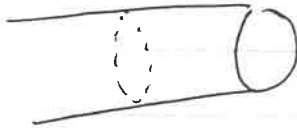
$$\frac{B_1}{\mu_1} = \frac{B_2}{\mu_2}$$

or if  $\mu_1 \gg \mu_2 (= \mu_0)$

$$B_2 = \frac{\mu_2}{\mu_1} B_1 \rightarrow 0$$

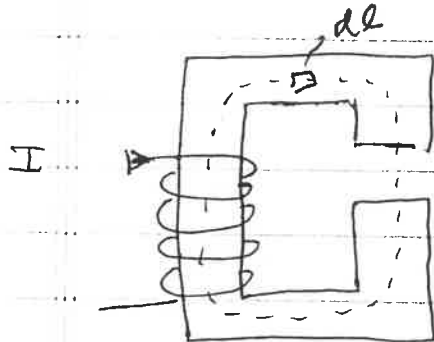
This says that  $B$  is inside, and since  $\Phi$  is conserved,

$$\Phi = B \cdot A \text{ or}$$



$$B = \frac{\Phi}{A} ; B \propto \frac{1}{\text{area}}$$

Now suppose the magnet is an electromagnet and is driven by  $N$  turns of current  $I$



We can integrate

$$\oint H \cdot dl = NI$$

and  $H(l) = \frac{\Phi}{\mu(l) A(l)}$

at a point  $l$  on the loop. This gives connection between  $\Phi$  &  $I$

$$\Phi \left[ \frac{1}{\mu} \int_{\text{core}} \frac{dl}{A(l)} + \frac{1}{\mu_0} \int_{\text{gap}} \frac{dl}{A(l)} \right] = NI$$



Now you can see a problem: what is  $A$  in the gap? Make some reasonable assumption (linear interpolation?) and go on.

but  
Since  $\mu \gg \mu_0$  the core term is negligible, then

$$\Phi \int_{\text{gap}} \frac{dl}{A(l)} = \mu_0 NI$$

$NI$  gives  $\Phi$  - and then  $B = \Phi/A$ .

This is why the tips are small - bigger  ~~$\Phi$~~   $B$ !

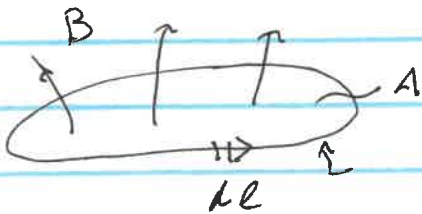
Magnetic Energy - slightly tricky

To create constant  $I$ 's &  $B$ 's requires transient time-varying fields. Faraday's law <sup>1</sup> tells us that  
(Maxwell eqn #4)

$$\vec{\nabla} \times \vec{E} + \frac{d\vec{B}}{dt} = 0$$

i.e. ~~time~~ time varying  $B \rightarrow$  circulatory  $E$

$$\int dA \left[ \vec{\nabla} \times \vec{E} + \frac{d\vec{B}}{dt} \right] \cdot \hat{n} = 0$$



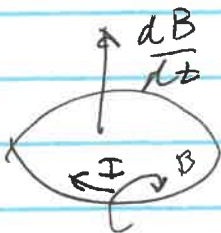
$$\oint \vec{E} \cdot d\vec{\ell} = - \frac{d}{dt} \int \vec{B} \cdot \hat{n} dA$$

voltage  $\equiv$  Electromotive Force ( $\mathcal{E} = - \int \vec{E} \cdot d\vec{\ell}$ )

$$\mathcal{E} = - \frac{d}{dt} \Phi_B$$

$=$  -time rate of change of magnetic flux.

Minus sign: Lenz's law: induced  $\mathcal{E}$  (and current, if wire has resistance) opposes change in flux



Induced EMF causes source of current to do work, which goes into energy budget.

The discussion of magnetic energy starts with the Lorentz force law for a charged particle

$$\vec{F} = q(\vec{E} + \vec{v} \times \vec{B})$$

The time rate of change in energy ~~of~~ <sup>of</sup> electron is

$$\frac{dW}{dt} = \vec{F} \cdot \vec{v} = q \vec{v} \cdot \vec{E} \quad \text{if } |q \vec{v}| = \text{current } I$$

~~$\vec{E}$  is induced by  $\dot{\Phi}_B$ . Sources do work to maintain the current.  $\dot{\Phi}_B$  induces currents opposing~~

Now we want to create a steady state current. There is an initial transient period as current rises from zero:  $\dot{\Phi}_B \neq 0$ , there is an induced EMF, sources do work to maintain the current ( $\dot{\Phi}_B$  induces currents opposing change in flux).

Work done by source to maintain ~~the~~ current =

$$= \frac{dW}{dt} = -I \mathcal{E} = -I \int \vec{E} \cdot d\vec{l} = I \frac{d\Phi_B}{dt}$$

$\uparrow$  Lenz's law       $\leftarrow$  work over circuit

$$\therefore \delta W = I \delta \Phi_B = \text{work done by external agent} \\ = \text{energy stored in system.}$$

Now compute work expended in building up a steady state current + field distribution. Do this adiabatically, so  $\vec{\nabla} \cdot \vec{J} = 0$ .

Consider a little current loop shaped like a doughnut



$\sim S = \text{surface area of loop}$

$\sigma = \text{cross section, } I = J \Delta \sigma$

$$\delta W = I \delta \Phi_B$$

$$\Delta(\delta W) = (J \Delta \sigma) \int \hat{n} \cdot \delta \vec{B} dS$$

↑ change in energy      ↑ change in area

$$\vec{B} = \vec{\nabla} \times \vec{A} \text{ so } \Delta(\delta W) = J \Delta \sigma \int (\vec{\nabla} \times \delta \vec{A}) \cdot \hat{n} dS$$

$$= J \Delta \sigma \oint \delta A \cdot dl$$

↑ circumference of doughnut

But  $\Delta \sigma \oint dl = \text{volume of doughnut}$



$$\delta W = \int \delta \vec{A} \cdot \vec{J} d^3x$$

and if  $\vec{A} \propto \vec{J}$        $W = \frac{1}{2} \int \vec{J} \cdot \vec{A} d^3x$

Now ~~consider~~ consider macroscopic  $E \ll M$ ,  $\vec{J}$  a macro current:  $\vec{\nabla} \times \vec{H} = \vec{J}$

$$\delta W = \int \delta \vec{A} \cdot (\vec{\nabla} \times \vec{H}) d^3x$$

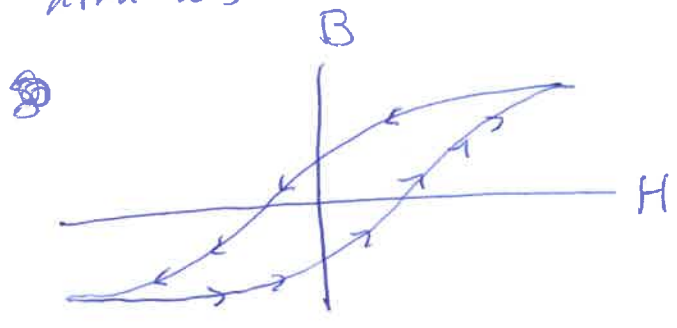
Vector identity  $\vec{\nabla} \cdot (\vec{P} \times \vec{Q}) = \vec{Q} \cdot (\vec{\nabla} \times \vec{P}) - \vec{P} \cdot (\vec{\nabla} \times \vec{Q})$

$\vec{Q} = \delta \vec{A}$     $\vec{P} = \vec{H}$

$\delta W = \int [\vec{H} \cdot (\vec{\nabla} \times \delta \vec{A}) + \vec{\nabla} \cdot (\vec{H} \times \delta \vec{A})] d^3x$   
*assume vanishes on surfaces*

$\delta W = \int \vec{H} \cdot \delta \vec{B} d^3x$  true in general

Example: hysteresis curve for real magnets -  
 M depends on past history of material  
 (magnetic domains ~~move~~ form and move around)



~~$\Delta U = \oint_{\text{closed path}} \vec{H} \cdot \delta \vec{B} dV = \oint \vec{B} \cdot \delta \vec{H} dV$~~

= ~~area under~~  $\oint \delta B \rightarrow \oint dB$   
 Cycle the magnet:  ~~$\oint \delta H \rightarrow \oint dH$~~

$\Delta U = \int dV \oint H \cdot dB = \int dV \oint B \cdot dH$

energy expended per unit volume  
 = area of hysteresis loop



(Recall similar formula for dielectric

$$\delta W = \int \vec{E} \cdot \delta \vec{D} d^3x)$$

For linear materials  $\vec{H} \cdot \delta \vec{B} = \frac{1}{2} \delta (\vec{H} \cdot \vec{B})$

$$W = \frac{1}{2} \int \vec{H} \cdot \vec{B} d^3x \rightarrow \underbrace{\left[ \frac{1}{2\mu_0} \int B^2 d^3x + \frac{\epsilon_0}{2} \int E^2 d^3x \right]}_{\text{energies in EM field}}$$

Variation on this story: what is the change in energy when a permeable material ( $\mu \neq \mu_0$ ) is placed in an external field, when currents are held constant?

before	after
$\mu_0$	$\mu$
$B_0$	$B$
$H_0$	$H$

Copy from the electrostatics problem

$$\vec{E} \cdot \delta \vec{D} \rightarrow \vec{E} \cdot \vec{D}_0 - \vec{D} \cdot \vec{E}_0$$

$$\vec{H} \cdot \delta \vec{B} \rightarrow \vec{H} \cdot \vec{B}_0 - \vec{B} \cdot \vec{H}_0$$

except - copy from case of fixed voltage / fixed sources - there is an extra minus sign

$$W = \frac{1}{2} \int_V d^3x \left[ \vec{B} \cdot \vec{H}_0 - \vec{H} \cdot \vec{B}_0 \right]$$

$$= \frac{1}{2} \int_V [\mu - \mu_0] \vec{H} \cdot \vec{H}_0 d^3x$$

$$= \frac{1}{2} \int \left[ \frac{1}{\mu_0} - \frac{1}{\mu} \right] \vec{B} \cdot \vec{B}_0 d^3x$$

$$\vec{B} = \mu_0 [\vec{H} + \vec{M}] \quad \therefore \frac{\vec{B}}{\mu_0} = \vec{H} + \vec{M} \Rightarrow \frac{\vec{B}}{\mu} = \vec{H}$$

$$W = \frac{1}{2} \int d^3x [\vec{H} + \vec{M} - \vec{H}] \cdot \vec{B}_0 = \frac{1}{2} \int d^3x \vec{M} \cdot \vec{B}_0$$

(contrast w/  $-\frac{1}{2} \int \vec{P} \cdot \vec{E} d^3x$ )

$W_{\text{mag}}$  = total energy change including work done against EMF - like electrostatics at fixed voltage.

Inductance, self-inductance, mutual inductance

Self-inductance  $L$ :  $\Phi_B = L \cdot I$

$\Phi_B$  = flux through circuit ~~carrying~~ carrying current  $I$

Then  $\delta W = I \delta \Phi_B = I \delta (LI) = \delta \left( \frac{1}{2} LI^2 \right)$

$$W = \frac{1}{2} LI^2 \quad (\text{like } \frac{1}{2} CV^2)$$

Mutual inductance:  $(\Phi_B)_1 = M_{12} I_2$

$(\Phi_B)_1$  = flux through circuit 1 due to  $I_2$  in circuit 2

Easy to show  $M_{12} = M_{21}$

$$\delta W_{12} = I_1 \delta (\Phi_B)_1 = I_1 \delta (M_{12} I_2) = M_{12} I_1 \delta I_2$$

$$W_{\text{TOT}} = \frac{1}{2} L_1 I_1^2 + M_{12} I_1 I_2 + \frac{1}{2} L_2 I_2^2$$

## Displacement Current

$$\nabla \cdot \left( \vec{\nabla} \times \vec{H} = \vec{J} \right) \Rightarrow 0 = \vec{\nabla} \cdot \vec{J}$$

but if there is time variation,  $\vec{\nabla} \cdot \vec{J} = -\frac{\partial \rho}{\partial t} \neq 0$   
inconsistent w/ charge conservation

Maxwell's great fix-up

$$\begin{aligned} 0 &= \vec{\nabla} \cdot \vec{J} + \frac{\partial \rho}{\partial t} = \vec{\nabla} \cdot \vec{J} + \frac{\partial}{\partial t} \vec{\nabla} \cdot \vec{D} \\ &= \vec{\nabla} \cdot \left[ \vec{J} + \frac{\partial \vec{D}}{\partial t} \right] \end{aligned}$$

← "displacement current"

then rewrite

$$\vec{\nabla} \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

Microscopic:  $\vec{\nabla} \times \vec{B} = \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$

~~Maxwell~~ Maxwell eqns:  $\vec{\nabla} \times \vec{E} + \frac{\partial \vec{B}}{\partial t} = 0$      $\vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon_0}$      $\vec{\nabla} \cdot \vec{B} = 0$

In free space  $\rho = 0$      $\vec{\nabla} \times (\vec{\nabla} \times \vec{B}) = \mu_0 \epsilon_0 \frac{\partial}{\partial t} (\vec{\nabla} \times \vec{E})$

$$\vec{\nabla} (\vec{\nabla} \cdot \vec{B}) - \nabla^2 \vec{B} = -\mu_0 \epsilon_0 \frac{\partial^2 \vec{B}}{\partial t^2}$$

$$\vec{\nabla}^2 \vec{B} - \mu_0 \epsilon_0 \frac{\partial^2 \vec{B}}{\partial t^2} = 0$$

Waves:  $\frac{1}{c^2} = \mu_0 \epsilon_0$

BTW solutions of wave eq are  
waves - in 1-d  $\left( \frac{\partial^2}{\partial x^2} - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} \right) f(x \pm ct) = 0$

Now need machinery to deal efficiently with EM radiation